SUPPLEMENTARY TRAFFIC STUDY BERRY HILLS PHASE 8



PREPARED FOR: ARMCO CAPITAL INC.

SEPTEMBER 3, 2019

Project No. 191-06902





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1 INTRODUCTION

Background

On March 1st, 2019, Armco Capital Inc. submitted a development application for Berry Hills Phase 8. That application was accompanied by a report titled *Berry Hills Phase 8 Traffic Impact Study* undertaken by Harbourside Transportation Consultants and dated February 12th, 2019.

A review was completed by HRM and, on April 17th, 2019 the applicant was provided with a memo from Sarah Rodger, Program Engineer dated April 17th, 2019. That memo included the line "Approval is not recommended until the first comment (regarding the TIS) is addressed". The purpose of this report is to address the specific comments raised in that memo.

This is not a full Traffic Impact Study but should be read as a supplement to the original Harbourside report. The assumptions, calculations and background traffic counts contained in the original report, other than those challenged in the HRM comments or as noted in this report, have been adopted for this analysis.

Addressing the Issues Raised

Following is a listing of the HRM comments on the Harbourside report and how those are addressed in this report:

- 1) "Identification of the transportation system changes needed to mitigate the impact of the proposed development on the transportation network have not been adequately addressed. The report findings show that the proposed development will significantly affect traffic operations. Although there are projected operational issues with background traffic growth, the additional site-generated traffic must not worsen the situation as required in section 6.3 of HRM's Guidelines for the Preparation of Transportation Impact Studies (8th Revision)."
 - This report introduces a plan to provide better access management control on Trunk 1 through the signalization of the Trunk 1/Lively Road intersection. The plan diverts traffic away from unsignalized intersections where stopped delay is significant to a signalized intersection that provides adequate level of service. Some of this diversion will occur naturally due to the desire of drivers to migrate towards the intersection with better service and safety and some will be forced through the redesign of the proposed subdivisions connections.
- 2) "The consultant did offer a potential solution of providing an alternate route into the development area through the construction of a fourth leg of the Sackville Drive/Margeson Drive roundabout. There was no data included to support this recommendation and it was not clear whether the Developer was proposing to build this connection. This road is not in the current capital budget. The road was listed in the last revision of the Regional Municipal Planning Strategy as a "Future Potential" road, meaning the project was identified to be constructed beyond the 25-year horizon of the 2006 Regional Plan. The Integrated Mobility Plan (IMP) has been approved by Regional Council, since the last revision of the Regional Plan. Transportation projects now consider the priorities of the IMP, which aims to limit the expansion of the road network."

- Construction of this connection by the developer is impractical and is not being proposed. Future construction of this roadway by the Municipality would provide a great opportunity to relieve traffic issues on Trunk 1 with a simple connection to Wilson Lake Drive. The plan described in this report does not rely, however, on this connection to adequately manage development traffic. It does not result in new roadway length being added, other than internal subdivision streets.
- 3) "Traffic volumes shown in Appendix C do not match those used in the traffic signal warrants. Are the traffic signal warrants completed for 2024 with or without the proposed development?"
 - This report assesses the warrants for traffic signals for a number of horizons and scenarios. This is well documented in the Appendix of this report.
- 4) "HRM will be implementing traffic calming measures (speed humps) on Wilson Lake Drive and Lively Road in 2019. As mentioned previously, the recommendation to install a compact roundabout on Wilson Lake Drive at the new intersection to the development would be strongly supported by HRM Traffic. This should also be taken into consideration on the Lively Road side of the development."
 - Consideration will be given to complimenting proposed traffic calming measures with design of the development roadways and connections.
- 5) "Intersection analysis results at Sackville Drive and Wilson Lake Drive have changed for existing conditions (2017) and future conditions without development since the original TIS. What changes were made to result in these?"
 - Redistribution of traffic that results from the plan proposed in this report reduces the traffic issues at this intersection.
- 6) "Multi-family housing (low rise) applies to housing units with at least 3 other units. I don't believe this is applicable to the semi-detached units (townhouses) in this case. Use of the single-family detached housing code results in a greater number of trips."
 - We support this comment and have recalculated development trip generation accordingly.

2 BACKGROUND DATA AND ACCESS MANAGEMENT PLAN

Development Site

The development site and general access plan has not changed from that shown in Figures 1 and 2 of the Harbourside study. The proposed development consists of 108 single family detached homes and 56 multi-family low-rise units.

Background Traffic Growth

An annual 1.5% growth in background traffic used in the Harbourside study was retained for this assessment.

Traffic Counts

To supplement the data collected in 2017 for the Harbourside study, WSP undertook a six-hour intersection turning movement count at the Rosemary Drive/Trunk 1 intersection on August 7th, 2019. Volumes on Trunk 1 are equivalent for both sets of counts so no factoring for the two-year gap was applied.

Collision History

HRM provided data acquired from the RCMP for the intersections at Wilson Lake Drive, Lively Road and Rosemary Drive for a three-year period ending July 2019. Three property damage collisions were recorded during that period, two of which can be linked to high stopped delay entering Trunk 1 from an unsignalized approach during peak hours:

- 1) Lively Road 8:05am Vehicle struck from behind while stopped on Trunk 1 allowing vehicles from Lively Rd. to exit onto Trunk 1, no injuries.
- 2) Wilson Lake Drive 4:45pm Vehicle turning left from Wilson Lake Dr. onto Trunk 1 struck oncoming Bedford bound vehicle, no injuries.

Access Plan

Our access management plan recognizes that a poor level of service is created with traffic attempting to make a left turn from a stop-controlled intersection leg on unsignalized intersections along Trunk 1. Collision history shows some collisions that occurred here are likely related to the difficulty vehicles experience turning onto Trunk 1 from these intersections. For these reasons, we have redesigned the connections from the development site to the roadway network to direct all trips exiting the site to Lively Road. We then propose to signalize the Lively Road/Trunk 1 intersection to safely manage this increased traffic. All trips entering the site will remain as modeled in the Harbourside study.

To achieve this, we will create the connection between Wilson Lake Drive and the development site as a one-way street into the site. All trips exiting the site will be required to use Lively Road. This plan will not affect emergency access into the site and will not force changes to existing traffic patterns (although we expect these patterns to change naturally once signalization is implemented).

This plan is shown in Figure 1.

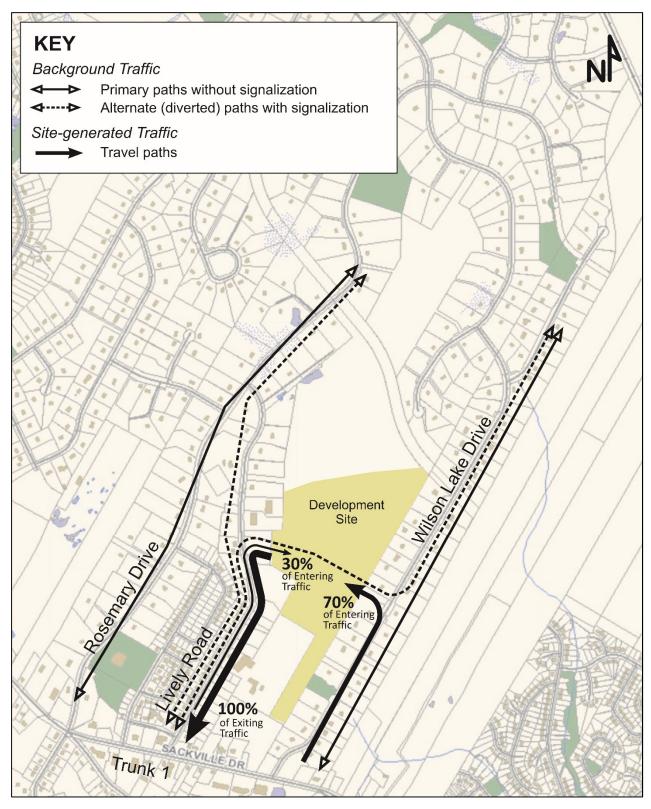


Figure 1: Travel Patterns and Trip Distribution

3 TRAFFIC ASSESSMENT

Trip Generation

Trip generation for the proposed development were taken from rates provided in the 10th edition of the *Trip Generation Manual* published by the Institute of Transportation Engineers. The results are shown in Table 1:

Table 1: Trip Generation Estimates

Land Use	Units		Trip Ge	neratio	n Rates		Т	rip Ger	eratio	n Estim	ates
		AM P	eak	PM I	Peak	Daily	AM	Peak	PM	Peak	Daily
		In	Out	In	Out	2way	In	Out	In	Out	2way
Single Family incl Small Multi-unit (Land Use 210)	164	0.18	0.56	0.64	0.36	9.44	30	92	105	59	1548

To assess the need for signalization, a six-hour count consisting of two AM peak hours, two mid-day hours, and two PM peak hours is required. These volumes are easily acquired for background traffic through field counts but are not available through trip generation tables. For this study, we have extrapolated the six-hour counts from the two peak hour generation counts based on patterns in our counted data. This relationship is shown in Table 2.

Table 2: Extrapolating Trip Generation Estimates into Six Hour Count

Count Required for Warrant Calculation	Count from ITE Trip Generation
1 st AM hour	AM Peak Hour
2 nd AM hour	85% of AM Peak Hour
1 st Mid-day hour	65% of AM Peak Hour
2 nd Mid-day hour	65% of PM Peak Hour
1 st PM hour	85% of PM Peak Hour
2 nd PM hour	PM Peak Hour

Trip Distribution and Assignment The Harbourside study assumed that 70% of the generated trips would use Wilson Lake Drive to access Trunk 1 and the remainder would use Lively Road. That distribution was adopted for this study, although only for traffic entering the site. With the proposed street connections, 100% of exiting traffic would use Lively Road.

The Harbourside study used existing patterns at each intersection to determine whether trips would be attracted to/produced from the east or the west resulting in the percentage of trips to/from the west varying anywhere from 7% to 28%. A more standard approach was taken in this analysis, still consistent with existing traffic patterns, that assumed 15% of all newly generated trips would come to/from the west and 85% of trips to/from the east.

Redistributing Background Traffic When several interconnected local or collector streets come out to a busy arterial street at unsignalized intersections, stopped delay will be high and traffic will naturally spread out evenly between streets to minimize that delay. When one of those intersections becomes signalized, traffic will naturally migrate towards that intersection to take advantage of the reduced delay and improved safety. The inter-connectedness of Rosemary Drive, Lively Road and Wilson Lake Drive means that signalization of the Lively Road intersection at Trunk 1 will result in traffic migrating to Lively Road from the other two streets. Since left turning traffic out of the stop-controlled street experiences the highest stopped delay, that is the traffic that is most likely to be diverted. To test the sensitivity of assumptions, two scenarios (see Table 3) were produced regarding the redistribution of traffic.

Table 3: Redistribution of Existing Traffic Resulting from Signalization

Street	Movement	Percentage Divert	ted to Lively Road
		High Scenario	Low Scenario
Rosemary Drive	Left Turns Out	60%	40%
	Left Turns In	20%	10%
	Right Turns Out	20%	10%
	Right Turns In	0%	0%
Wilson Lake Drive	Left Turns Out	60%	40%
	Left Turns In	20%	10%
	Right Turns Out	20%	10%
	Right Turns In	0%	0%

Projected Traffic Volumes Trips generated by the proposed development were added to the projected background volumes to provide projected AM and PM peak hourly and six-hour traffic volumes illustrated diagrammatically in the Appendix.

4 RESULTS

Traffic Signal Warrant

The Canadian Traffic Signal Warrant Matrix Analysis (Transportation Association of Canada (TAC), 2005) considers 100 warrant points as an indication that traffic signals will provide a positive impact. Signal warrant analysis uses vehicular and pedestrian volumes, and intersection, roadway and study area characteristics to calculate a warrant point value. That warrant calculation was applied to the Lively Road intersection with the results shown in Table 4.

Scenario	Signal Priority Points
2018/19 without development	55
2024 without development/high redistribution	66
2024 with development/high redistribution	103

2024 with development/low redistribution

Table 4: Two-way Daily Volumes on Key Collector and Local Streets

These results indicate that signalization at Lively Road will be warranted at full build-out of the development. Even with a lower redistribution assumption, signalization should still be considered necessary. Although signalization is not strictly warranted at the development start-up, it would be appropriate to install signalization at that point in anticipation of its impending need.

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Intersection Capacity Analysis Results Synchro 10.0 was used for performance evaluation of a signalized Lively Road/Trunk 1 intersection using projected design hourly volumes with the site development. Analysis results are included in the Appendix and indicate that the intersection will operate at a satisfactory level of service (level of service 'B') using the intersection configuration shown in Figure 2.

The capacity of the Wilson Lake Drive unsignalized intersection was not assessed. Since access to the signalized intersection at Lively Road with reduced delay is readily available, any level of service issues for Wilson Lake Drive will "self-correct" with traffic shifting to Lively Road.

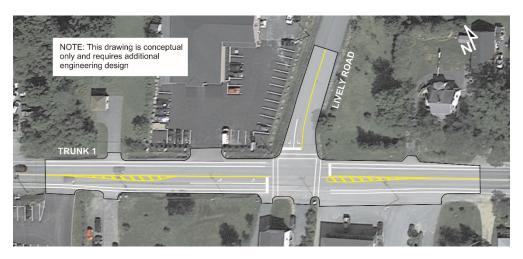


Figure 2: Conceptual Layout of Lively/Trunk 1 Intersection

5 RECOMMENDATIONS

Site Roadway Connections To help guide traffic exiting the proposed develop and areas around it to Lively Road where better level of service is provided, it is recommended that the connection between the development site and Wilson Lake Drive be one-way westbound (inbound to the development).

Figure 3 shows conceptually how that roadway would be designed and signed to enforce one-way flow.

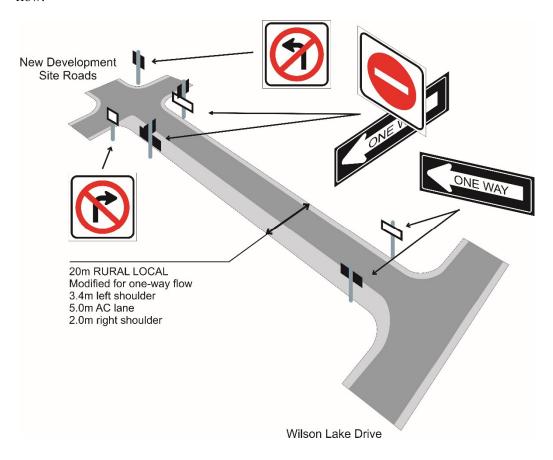


Figure 3: Proposed Layout of One-way Connection to Wilson Lake Drive

Lively Road/ Trunk 1 Intersection The results of our analysis indicate that signalization at Lively Road will be warranted at full build-out of the development. Even with a lower redistribution assumption, signalization should still be considered necessary.

The intersection should be modified to create a left turn storage lane on Trunk 1 and a right turn bay on the Lively Road approach. A schematic of the intersection layout is provided in Figure 2. Queue storage lengths are based on the Synchro modeling results.

APPENDIX

TRAFFIC VOLUME DATA AND MODELLING RESULTS

Exhibit A-1 Turning Movement Count – Trunk 1 @ Rosemary Drive

	Tab	le A-1						
	Tri	unk 1						
		@				A C		
	Rosem	ary Drive	,					
							L D	
							— E	
					L -4			
		Sackville, NS			к 🗪			
	Wednesday	, August 7, 2019		_				
			AM Pea	k Period Vo	lume Data			
			ary Drive	Trur			nk 1	Total
Т	ime		d Approach	Westbound			Approach	Vehicles
07:00	07:15	0 0	C 17	D 2	E 33	95	L 3	150
07:15	07:30	1	14	3	23	119	1	161
07:30	07:45	3	17	2	39	127	1	189
07:45 08:00	08:00 08:15	2	15 15	3 6	33 35	100 106	0 2	153 165
08:00	08:15	1	10	2	55 55	107	1	176
08:30	08:45	0	6	4	52	100	4	166
08:45	09:00	1 7	9	4	60	79	1	154
AM Pe 07:00	ak Hour 08:00	7	57 63	13 10	162 128	440 441	5	683 653
08:00	09:00	3	40	16	202	392	8	661
		P	ed 1	Ped	d 3	Pe	d 4	Total Ped
07:00	08:00		0	C			0	0
08:00	09:00		0	C			0	0
			Midday P	eak Period V	olume Data			
			ary Drive	Trur			nk 1	Total
Т	ime	Northbour A	d Approach B	Southbound H	Approach	Eastbound J	Approach L	Vehicles
11:00	11:15	0	5	11	62	87	0	165
11:15	11:30	1	5	6	76	74	2	164
11:30	11:45	0	12	5	73	98	2	190
11:45 12:00	12:00 12:15	0	3 7	6 4	79 87	79 67	1 2	168 168
12:15	12:30	1	6	4	77	74	1	163
	12:45	0	9	5	85	65	1	165
12:30	13:00	5	6	5	74	59	1	150
12:30 12:45					0.45	0.40	_	690
12:45 Midday F	Peak Hour	2	27	21	315 290	318 338	7	
12:45 Midday F 11:00	Peak Hour 12:00 13:00	1 7	27 25 28	21 28 18	315 290 323	318 338 265	7 5 5	687 646
12:45	12:00	1 7	25	28	290 323	338 265	5	687 646
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Exhibit A-2 Traffic Distribution Model

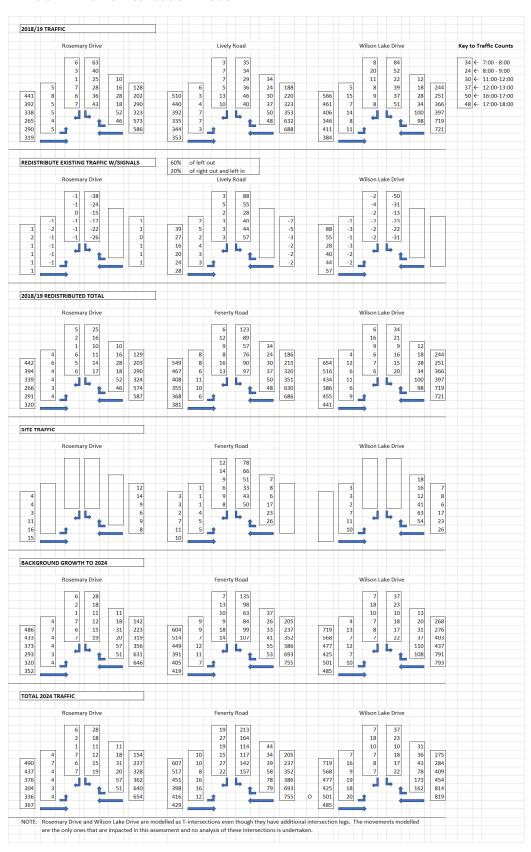


Exhibit A-3 Signal Warrant Calculation – 2019 Traffic

Main Street (name))	Trunk 1			ction (EV		EW				Date:						
Side Street (name)	Fe	nerty Ro	ad	Dire	ction (EV	V or NS)	NS				City:						
Quadrant (if appl)																
								anes									
ane Configuration		Exel LT	Th & LT	Through or Th+RT+LT	Th & RT	Excl RT	UpStream Signal (m)	# of Thru Lanes									
Trunk 1	WB	1		1				1				Demogra					
Trunk 1 Fenerty Road	EB NB				1			1				Elementar Senior's C			(y/n) (y/n)	y	
Fenerty Road	SB	1				1						Pathway t			(y/n)	n y	
, , , , , , , , , , , , , , , , , , , ,												Metro Are	a Populatio		(#)	10	
												Central B	isiness Dis	trict	(y/n)	n	
ther input		Speed (Km/h)	Trucks	Bus Rt (y/n)	Median (m)												
Trunk 1	EW	70	2.0%	у у	0.0												
Fenerty Road	NS		0	n									D 14	D 10	D 12	D 14	
raffic Input		NB			SB			WB			EB		Ped1 NS	Ped2 NS	Ped3 EW	Ped4 EW	
rame input	LT	Th	RT	LT	Th	RT	LT	Th	RT	LT	Th	RT	W Side	E Side	N Side	S side	
7:30 - 8:30	LI	. 111	K1	123	111	6	LI	186	49	8	549	K1	** Side	E Side	14 Side	5 side	
8:30 - 9:30				89		12		215	36	8	467						
11:30 - 12:30				57		9		320	41	6	408						
12:30 - 13:30				76		8		351	67	11	355						
16:00 - 17:00				90		16		630	95	10	368						
17:00 - 18:00				97		13		686	89								
										1 6	381						
Total (6-hour peak)	0	0	0		0		0			6 49	381 2,528	0	0	0	0	0	
Total (6-hour peak) Average (6-hour peak)	0	0	0	532 89	0	64	0	2,388 398	377 63	49 8	2,528 421	0	0	0	0	0	
	0			532		64		2,388	377 63	49	2,528 421	0	0	0		0	х С _і
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Average (6-hour peak) Average 6-hour Peak Turning	<	0	409	532 89	RT	88 66 HL	LT	2,388 398	377 63 4H20N 8N	49	2,528 421 W = [O C _{bt} (X _v	0 W = NOT	0 1 + (F (Warra	0 (X _{v-p}) L)	0 / K ₂] x	0
Average (6-hour peak) Average 6-hour Peak Turning	Trunk 1	WB	409	532 89	RT	88 66 HL	LT	2,388 398	377 63 4H20N 8N	49	2,528 421 W = [C _{bt} (X,	0 W = NOT 461 Trunk 1	0 1 + (F (Warra	0 (X _{v-p}) L)	0 / K ₂] x	0
Average (6-hour peak) Average 6-hour Peak Turning	Trunk 1	WB	409 LT TH	532 89	RT	88 66 HL	LT	2,388 398	377 63 4H20N 8N	49	2,528 421 W = [C _{bt} (X,	0 W = NOT 461 Trunk 1	0 1 + (F (Warra	0 (X _{v-p}) L)	0 / K ₂] x	0
Average (6-hour peak) Average 6-hour Peak Turning	Trunk 1	WB	409 LT TH	532 89	RT	88 66 HL	LT	2,388 398 Henerty Road	STORY OF THE STORY	8	2,528 421 W = [C _{bt} (X,	0 W = NOT 461 Trunk 1	0 1 + (F (Warra	0 (X _{v-p}) L)	0 / K ₂] x	0
Average (6-hour peak) Average 6-hour Peak Turning	Trunk 1	WB	409 LT TH	532 89	RT	88 66 HIL 0	LT	2,388 398 Lenerty Road	o c	8	2,528 421 W = [C _{bt} (X,	0 W = NOT 461 Trunk 1	0 1 + (F (Warra	0 (X _{v-p}) L)	0 / K ₂] x	0
Average (6-hour peak) Average 6-hour Peak Turning	Trunk 1	WB	409 LT TH	532 89	RT	88 66 HL 0	LT	2,388 398 Lenerty Road	377 63 CHUON BN IL	8	2,528 421 W = [C _{bt} (X,	0 W = NOT 461 Trunk 1	0 1 + (F (Warra	0 (X _{v-p}) L)	0 / K ₂] x	0

Exhibit A-4 – Signal Warrant Calculation – 2024 Without Site Traffic

Main Street (name)		Trunk 1		Dire	ction (EV	V or NS)	EW				Date:						
Side Street (name)	Fe	enerty Ro	oad	Dire	ction (EV	V or NS)	NS				City:						
Quadrant (if appl)																	
								anes									
ane Configuration		Excl LT	Th & LT	Through or Th+RT+LT	Th & RT	Excl RT	UpStream Signal (m)	# of Thru Lan									
Trunk 1 Trunk 1	WB EB	1		1	1			1				Demogra Elementar			(y/n)	v	
Fenerty Road	NB				•							Senior's C			(y/n)	n	
Fenerty Road	SB	1				1						Pathway t	o School		(y/n)	y 10	
													ea Populatio usiness Dis		(#) (y/n)	n	
Other input		Speed (Km/h)	Trucks	Bus Rt (y/n)	Median (m)												
Trunk 1	EW	70	2.0%	у	0.0												
Fenerty Road	NS		0	n									Ped1	Ped2	Ped3	Ped4	
raffic Input		NB			SB			WB			EB		NS	NS	EW	EW	
<u> </u>	LT	Th	RT	LT	Th	RT	LT	Th	RT	LT	Th	RT	W Side	E Side	N Side	S side	
7:30 - 8:30				135		7		205	37	9	604						
8:30 - 9:30				98		13		237	26	9	514						
11:30 - 12:30				63		10		352	33	7	449						
12:30 - 13:30				84		9		386	41	12	391						
16:00 - 17:00				99		18		693	55	11	405						
17:00 - 18:00	0	0	0	107	0	14	0	755	53	7	419	0	0	0	0	0	
Total (6-hour peak) Average (6-hour peak)	0	0	0	107 586 98	0	14 71 12	0	2,628 438	53 245 41	7 55 9	419 2,782 464	0	0	0	0	0	
Total (6-hour peak) Average (6-hour peak)	0			586		71 12		2,628	245 41	55	2,782 464	0	0	0		0	ı C _i
Total (6-hour peak) Average (6-hour peak) Average 6-hour Peak Turning	0			586 98		71		2,628 438	245	55	2,782 464	0	0	0 1 + (F (0	0	«C _i
Total (6-hour peak) Average (6-hour peak) Average 6-hour Peak Turning	0			586		71 12		2,628 438	245 41	55	2,782 464	0	0 _{/-V}) / K	0 1 + (F (0 (X _{v-p}) L	0 / K ₂] x	
Total (6-hour peak) Average (6-hour peak) Average 6-hour Peak Turning	0			586 98	0	71 12 88 01	0	2,628 438	245 41 Au Au Au Au Au Au Au Au Au Au Au Au Au	55	2,782 464	0	0 /-v) / K	0 1 + (F (0 [X _{v-p}] L]	0 / K ₂] x	0
Total (6-hour peak) Average (6-hour peak) Average 6-hour Peak Turning	0			586 98	RT	71 12 88 011 HL	LT	2,628 438	245 41 Au Au Au Au Au Au Au Au Au Au Au Au Au	55	2,782 464	0	0 /-v) / K	0 1 + (F (0 [X _{v-p}] L]	0 / K ₂] x	0
Total (6-hour peak) Average (6-hour peak) Average 6-hour Peak Turning	0	0		586 98	RT	71 12 88 011 HL	LT	2,628 438	245 41 Au Au Au Au Au Au Au Au Au Au Au Au Au	55	2,782 464 W = [C _{bt} (X _v	0 /-v) / K	0 1 + (F (0 [X _{v-p}] L]	0 / K ₂] x	0
Total (6-hour peak) Average (6-hour peak) Average 6-hour Peak Turning	0	WB	0	586 98	RT	71 12 88 011 HL	LT	2,628 438	245 41 Au Au Au Au Au Au Au Au Au Au Au Au Au	55	2,782 464 W = [C _{bt} (X _v	0 V-v) / K W =	0 1 + (F (0 [X _{v-p}] L]	0 / K ₂] x	0
Total (6-hour peak) Average (6-hour peak) Average 6-hour Peak Turning	0	WB	0	586 98	RT	71 12 88 011 HL	LT	2,628 438	245 41 Au Au Au Au Au Au Au Au Au Au Au Au Au	55	2,782 464 W = [C _{bt} (X _v	0 V-v) / K W =	0 1 + (F (0 [X _{v-p}] L]	0 / K ₂] x	0
Total (6-hour peak) Average (6-hour peak) Average 6-hour Peak Turning	0	WB	450	586 98 Ipad	RT	71 12 88 011 HL	LT	2,628 438	245 41 Au Au Au Au Au Au Au Au Au Au Au Au Au	55	2,782 464 W = [C _{bt} (X _v	0 W = NOT 479	0 1 + (F (0 [X _{v-p}] L]	0 / K ₂] x	0
Total (6-hour peak) Average (6-hour peak) Average 6-hour Peak Turning	o Trunk 1	WB	450	586 98	RT	71 12 88 011 HL	LT	2,628 438	245 41 Au Au Au Au Au Au Au Au Au Au Au Au Au	55	2,782 464 W = [C _{bt} (X _v	0 W = NOT 479	Warra	0 [X _{v-p}] L]	0 / K ₂] x	0
Total (6-hour peak) Average (6-hour peak) Average 6-hour Peak Turning	o Trunk 1	WB	450 LT TH	586 98 IPpad O	RT	71 12 88 011 HL	LT	Fenerty Road	245 41 41 41 08 09	55 9	2,782 464 W = [41 438 0	C _{bt} (X _v	0 W = NOT 479	Warra	0 [X _{v-p}] L]	0 / K ₂] x	0
Total (6-hour peak) Average (6-hour peak) Average 6-hour Peak Turning	o Trunk 1	WB	450 LT TH	586 98 IPpad O	RT	71 12 88 011 HL	LT	Fenerty Road	245 41 C4HUON BN 095	55 9	2,782 464 W = [C _{bt} (X _v	0 W = NOT 479	Warra	0 [X _{v-p}] L]	0 / K ₂] x	0
Total (6-hour peak) Average (6-hour peak) Average 6-hour Peak Turning	o Trunk 1	WB	450 LT TH	586 98 IPpad O	RT	71 12 88 011 HL	LT	Fenerty Road	245 41 41 41 08 09	55 9	2,782 464 W = [41 438 0	C _{bt} (X _v	0 W = NOT 479	Warra	0 [X _{v-p}] L]	0 / K ₂] x	0

Exhibit A-5 – Signal Warrant Calculation – 2024 With Site Traffic (High Redistribution)

Main Street (name)																	
		Trunk 1		Dire	ction (EV	V or NS)	EW				Date:						
Side Street (name)	Fe	nerty Ro	ad	Dire	ction (EV	V or NS)	NS				City:						
Quadrant (if appl)																	
								nes									
ane Configuration		ExclLT	Th & LT	Through or Th+RT+LT	Th & RT	Exel RT	UpStream Signal (m)	# of Thru Lane									
Trunk 1 Trunk 1	WB EB	1		1	1			1				Demogra Elementar			(y/n)	V	
Fenerty Road	NB				1			1				Senior's C			(y/n) (y/n)	y n	
Fenerty Road	SB	1				1						Pathway t	o School		(y/n)	у	
													a Populations in Population		(#) (y/n)	10 n	
												Cellual B	ISINGSS DIS	uici	(y/II)	п	
ther input		Speed (Km/h)	Trucks	Bus Rt (y/n)	Median (m)												
Trunk 1	EW	70	2.0%	у	0.0												
Fenerty Road	NS		0	n									Ped1	Ped2	Ped3	Ped4	
raffic Input		NB			SB			WB			EB		NS	NS	EW	EW	
	LT	Th	RT	LT	Th	RT	LT	Th	RT	LT	Th	RT	W Side	E Side	N Side	S side	
7:30 - 8:30				213		19		205	44	10	607						
8:30 - 9:30				164		27		237	34	10	517						
11:30 - 12:30				114		19		352	39	8	451						
12:30 - 13:30				117		15		386	58	16	396						
16:00 - 17:00				142		27		693	78	16	416						
17:00 - 18:00				157		22		755	79	12	429						
Total (6-hour peak)	0	0	0	907	0	129	0	2,628	332	72	2,816	0	0	0	0	0	
Average (6-hour peak)	0	0	0	151	0	22	0	438	55	12	469	0	0	0	0	0	
Average 6-hour Peak Turning								_									
Movements						SB		Fenerty Road	North>		W =	C _{bt} (X _v			(X _{v-p}) L)		
_						173 SB		Fenerty Road	NB North>		W =	C _{bt} (X _v	W =		(X _{v-p}) L)	103	0
_				Ped1	RT		LT	Fenerty Road	67 NB North>		W =	C _{bt} (X _v					
_				0 Ped1	. 22 RT	173	151 LT	Fenerty Road	N N		W =	C _{bt} (X _v	W =			103	0
_						TH 173		Fenerty Road	N N		W =	C _{bt} (X _v	W =	1		103	0
	<	WB	460			TH 173		Fenerty Road	N N		1		W =	1		103	0
Movements	< Trunk 1	WB	460			TH 173		Fenerty Road	N N		- 55	RT	W =	1 canted		103	0
Movements		WB	460			TH 173		Fenerty Road	N N		55 438	RT TH	W =	ranted WB		103	0
Movements		WB 481		0		TH 173		Fenerty Road	ZB		55 438	RT TH	W = Warr 493 Trunk 1	ranted WB		103	0
Movements	Trunk 1		LT	12		TH 173		Fenerty Road	ZB		55 438	RT TH LT	W = Warr 493 Trunk 1	ranted wb		103	0
Movements	Trunk 1		LT TH	12 469		TH 173		0 Fenerty Road	ZB	0	55 438	RT TH LT	W = Warr 493 Trunk 1	ranted wb		103	0
Movements	Trunk 1		LT TH	12 469		TH 173		0	NB 67 NB		55 438 0	RT TH LT	W = Warr 493 Trunk 1	ranted wb		103	0
Movements	Trunk 1		LT TH	12 469		0 TH 173			0 0 0	RT 0	55 438 0	RT TH LT	W = Warr 493 Trunk 1	ranted wb		103	0

Exhibit A-6 – Traffic Signal Warrant – 2024 With Site Traffic (Low Redistribution)

	Cana																
Main Street (name)		Trunk 1		Dire	ction (EV	V or NS)	EW				Date:						
Side Street (name)	Fe	nerty Ro	ad	Dire	ction (EV	V or NS)	NS				City:						
Quadrant (if appl))																
								e e									
ane Configuration		Exel LT	Th & LT	Through or Th+RT+LT	Th & RT	Exel RT	UpStream Signal (m)	# of Thru Lanes									
Trunk 1	WB	1		1				1				Demogra			(/)		
Trunk 1 Fenerty Road	EB NB				1			1				Elementar Senior's C			(y/n) (y/n)	y n	
Fenerty Road	SB	1				1						Pathway t			(y/n)	у	
													a Populatio		(#)	10	
												Central B	isiness Dis	trict	(y/n)	n	
ther input		Speed	Trucks	Bus Rt	Median												
Tenel: 1	EW	(Km/h)	2.0%	(y/n)	(m) 0.0												
Trunk 1 Fenerty Road	NS	70	0	n	0.0												
													Ped1	Ped2	Ped3	Ped4	
raffic Input		NB			SB			WB			EB		NS	NS	EW	EW	
	LT	Th	RT	LT	Th	RT	LT	Th	RT	LT	Th	RT	W Side	E Side	N Side	S side	
7:30 - 8:30				181		18		205	44	10	586						
8:30 - 9:30				144		24		237	34	8	502						
11:30 - 12:30				104		18		352	39	8	443						
12:30 - 13:30 16:00 - 17:00				102		14		386	58	14	383						
				126		26		693	78	14	401						
17:00 - 18:00	0	0	0	135	0	21	0	755	79	11	421	0	0	0	0	0	
	0	0	0		0		0	755 2,628 438				0	0	0	0	0	
17:00 - 18:00 Total (6-hour peak) Average (6-hour peak) Average 6-hour	0			135 792		21 121 20		755 2,628	79 332 55	11 65	421 2,736 456	0	0	0		0	ı C _i
17:00 - 18:00 Total (6-hour peak) Average (6-hour peak) Average 6-hour Peak Turning	0			135 792		21 121		755 2,628 438	79 332	11 65	421 2,736 456	0	0	0 1 + (F (0	0	C _i
17:00 - 18:00 Total (6-hour peak) Average (6-hour peak) Average 6-hour Peak Turning	0			135 792 132		21 121 20		755 2,628 438	79 332 55	11 65	421 2,736 456	0	0 (-v) / K	0 1 + (F ((X _{v-p}) L	0 / K ₂] x	0
17:00 - 18:00 Total (6-hour peak) Average (6-hour peak) Average 6-hour Peak Turning	0			135 792	0	21 121 20 89 80 80	0	755 2,628 438	79 332 55	11 65	421 2,736 456	0	0 V-v) / K	0 1 + (F (0 (X _{v-p}) L)	0 / K ₂] x	0
17:00 - 18:00 Total (6-hour peak) Average (6-hour peak) Average 6-hour Peak Turning	0			135 792 132	RT	21 121 20 88 85 41 HL	LT	755 2,628 438	79 332 55	11 65	421 2,736 456	0	0 V-v) / K	1 + (F (0 (X _{v-p}) L)	0 / K ₂] x	0
17:00 - 18:00 Total (6-hour peak) Average (6-hour peak) Average 6-hour Peak Turning	0	0		135 792 132	RT	21 121 20 88 85 41 HL	LT	755 2,628 438	79 332 55	11 65	421 2,736 456 W = [C _{bt} (X,	0 V-v) / K	1 + (F (0 (X _{v-p}) L)	0 / K ₂] x	0
17:00 - 18:00 Total (6-hour peak) Average (6-hour peak) Average 6-hour Peak Turning	0	0	0	135 792 132	RT	21 121 20 88 85 41 HL	LT	755 2,628 438	79 332 55	11 65	421 2,736 456 W = [C _{bt} (X _v	0 W =	0 1 + (F (0 (X _{v-p}) L)	0 / K ₂] x	0
17:00 - 18:00 Total (6-hour peak) Average (6-hour peak) Average 6-hour Peak Turning	<	0	0	135 792 132	RT	21 121 20 88 85 41 HL	LT	755 2,628 438	79 332 55	11 65	421 2,736 456 W = [C _{bt} (X _v	0 W =	0 1 + (F (0 (X _{v-p}) L)	0 / K ₂] x	0
17:00 - 18:00 Total (6-hour peak) Average (6-hour peak) Average 6-hour Peak Turning	<	0	458	135 792 132	RT	21 121 20 88 85 41 HL	LT	755 2,628 438	79 332 55	11 65	421 2,736 456 W = [C _{bt} (X _v	0 W = NOT 493	0 1 + (F (0 (X _{v-p}) L)	0 / K ₂] x	
17:00 - 18:00 Total (6-hour peak) Average (6-hour peak) Average 6-hour Peak Turning	o <	WB	458	135 792 132	RT	21 121 20 88 85 41 HL	LT	755 2,628 438	79 332 55	11 65	421 2,736 456 W = [C _{bt} (X,	0 W = NOT 493	0 1 + (F (Warra WB	0 (X _{v-p}) L)	0 / K ₂] x	0
17:00 - 18:00 Total (6-hour peak) Average (6-hour peak) Average 6-hour Peak Turning	o <	WB	458 LT TH	135 792 132 132	RT	21 121 20 88 85 41 HL	LT	755 2,628 438	79 332 55	11 65	421 2,736 456 W = [C _{bt} (X,	0 W = NOT 493	0 1 + (F (Warra WB	0 (X _{v-p}) L)	0 / K ₂] x	0
17:00 - 18:00 Total (6-hour peak) Average (6-hour peak) Average 6-hour Peak Turning	o <	WB	458 LT TH	135 792 132 132	RT	21 121 20 88 85 41 HL	LT	755 2,628 438 Lenerty Road	79 332 55	11 65 11	421 2,736 456 W = [C _{bt} (X,	0 W = NOT 493	0 1 + (F (Warra WB	0 (X _{v-p}) L)	0 / K ₂] x	0
17:00 - 18:00 Total (6-hour peak) Average (6-hour peak) Average 6-hour Peak Turning	o <	WB	458 LT TH	135 792 132 132	RT	21 121 20 8S 751 HL	LT	755 2,628 438 Page Atheres Ath	79 3332 55 Authon 8N	11 65 11	421 2,736 456 W = [C _{bt} (X,	0 W = NOT 493	0 1 + (F (Warra WB	0 (X _{v-p}) L)	0 / K ₂] x	0

Trunk 7 & Lively Road

Page 1 AM Peak Hour

	•	<u> </u>	←	4	1	4
Lane Group	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	ሻ		1>		ሻ	7
Traffic Volume (vph)	10	607	237	44	213	27
Future Volume (vph)	10	607	237	44	213	27
Satd. Flow (prot)	1770	1863	1824	0	1770	1583
Flt Permitted	0.564	1003	1024	U	0.950	1000
		4000	4004	0	1770	4500
Satd. Flow (perm)	1051	1863	1824	0	1770	1583
Satd. Flow (RTOR)			20	•	000	29
Lane Group Flow (vph)	_ 11	660	306	0	232	29
Turn Type	Perm	NA	NA		Prot	Perm
Protected Phases		2	6		4	
Permitted Phases	2					4
Total Split (s)	62.0	62.0	62.0		28.0	28.0
Total Lost Time (s)	6.0	6.0	6.0		6.0	6.0
Act Effct Green (s)	56.0	56.0	56.0		22.0	22.0
Actuated g/C Ratio	0.62	0.62	0.62		0.24	0.24
v/c Ratio	0.02	0.57	0.27		0.54	0.07
Control Delay	6.6	12.4	7.9		34.9	10.5
Queue Delay	0.0	0.0	0.0		0.0	0.0
Total Delay	6.6	12.4	7.9		34.9	10.5
LOS	Α	В	Α		С	В
Approach Delay		12.3	7.9		32.2	
Approach LOS		В	Α		С	
Queue Length 50th (m)	0.7	63.7	21.1		36.8	0.0
Queue Length 95th (m)	2.7	94.1	34.0		60.3	6.8
Internal Link Dist (m)	2.7	336.5	345.9		279.0	0.0
Turn Bay Length (m)	30.0	000.0	040.0		210.0	30.0
Base Capacity (vph)	653	1159	1142		432	408
Starvation Cap Reductn	033	0	0		0	400
Spillback Cap Reductin	0	0	0		0	0
	0	0	0			0
Storage Cap Reductn Reduced v/c Ratio		0.57	0.27		0	
Reduced V/C Ratio	0.02	0.57	0.27		0.54	0.07
Intersection Summary						

Intersection Summary Cycle Length: 90

Actuated Cycle Length: 90
Offset: 0 (0%), Referenced to phase 2:EBTL and 6:WBT, Start of Green

Control Type: Pretimed Maximum v/c Ratio: 0.57 Intersection Signal Delay: 15.4 Intersection Capacity Utilization 53.7%

Intersection LOS: B ICU Level of Service A

Analysis Period (min) 15

Splits and Phases: 3: Trunk 7 & Lively Road



WSP Canada Inc.

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Trunk 7 & Lively Road

Page 2 PM Peak Hour

	۶	→	←	•	\	4
Lane Group	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	ሻ	†	(Î		ሻ	7
Traffic Volume (vph)	16	429	755	79	157	27
Future Volume (vph)	16	429	755	79	157	27
Satd. Flow (prot)	1770	1863	1839	0	1770	1583
Flt Permitted	0.161			-	0.950	
Satd. Flow (perm)	300	1863	1839	0	1770	1583
Satd. Flow (RTOR)			11	_		29
Lane Group Flow (vph)	17	466	907	0	171	29
Turn Type	Perm	NA	NA		Prot	Perm
Protected Phases		2	6		4	
Permitted Phases	2					4
Total Split (s)	62.0	62.0	62.0		28.0	28.0
Total Lost Time (s)	6.0	6.0	6.0		6.0	6.0
Act Effct Green (s)	56.0	56.0	56.0		22.0	22.0
Actuated g/C Ratio	0.62	0.62	0.62		0.24	0.24
v/c Ratio	0.09	0.40	0.79		0.40	0.07
Control Delay	8.3	9.9	18.9		31.7	10.5
Queue Delay	0.0	0.0	0.0		0.0	0.0
Total Delay	8.3	9.9	18.9		31.7	10.5
LOS	Α	Α	В		С	В
Approach Delay		9.8	18.9		28.7	
Approach LOS		Α	В		С	
Queue Length 50th (m)	1.1	38.7	109.7		26.1	0.0
Queue Length 95th (m)	4.1	58.1	167.9		45.1	6.8
Internal Link Dist (m)		336.5	345.9		279.0	
Turn Bay Length (m)	30.0					30.0
Base Capacity (vph)	186	1159	1148		432	408
Starvation Cap Reductn	0	0	0		0	0
Spillback Cap Reductn	0	0	0		0	0
Storage Cap Reductn	0	0	0		0	0
Reduced v/c Ratio	0.09	0.40	0.79		0.40	0.07
Intersection Summary						

Intersection Summary

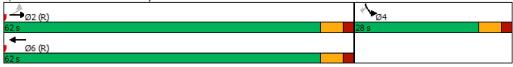
Cycle Length: 90
Actuated Cycle Length: 90
Offset: 0 (0%), Referenced to phase 2:EBTL and 6:WBT, Start of Green

Control Type: Pretimed
Maximum v/c Ratio: 0.79 Intersection Signal Delay: 17.4 Intersection Capacity Utilization 63.2%

Intersection LOS: B ICU Level of Service B

Analysis Period (min) 15

Splits and Phases: 3: Trunk 7 & Lively Road



WSP Canada Inc.

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