Transportation Impact Study
Wyse Road, Dartmouth
a report by Fathom Studio

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Project
Wyse Road,
Multi-Unit Development

Prepared for
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## TABLE OF CONTENTS

1. Introduction ..... 1
2. Existing Conditions ..... 2
2.1 Study Area ..... 2
2.2 Roadways and Intersections ..... 3
2.3 Active Transportation (AT) ..... 5
2.4 Vehicle Traffic .....  5
2.5 Transit ..... 6
2.6 Truck Routes .....  6
3. Future Conditions ..... 7
3.1 Context .....  7
3.1.1 Analysis Time Horizon ..... 7
3.1.2 Background Traffic .....  7
3.1.3 Analysis Period .....  8
3.2 The Development .....  8
3.2.1 Trip Generation .....  8
3.3 Trip Distribution and Assignment .....  9
3.3.1 Driveway Location ..... 9
4. Analysis ..... 10
4.1 Transportation Modelling ..... 10
4.2 Development Driveway ..... 10
4.3 Nantucket Ave/Sportsplex/Mall Driveway ..... 11
4.4 Nantucket Ave. / Victoria Rd. / School St ..... 12
4.5 Wyse Rd / Macdonald Bridge / Nantucket ..... 13
4.6 Wyse Road and Thistle Street ..... 15
5. Conclusions ..... 17
APPENDICIES
Appendix A: Traffic Counts
Appendix B: Trip Generation
Appendix C: Trip Assignment
Appendix D: Synchro Output
Appendix E: Alternate Driveway Evaluation

## INTRODUCTION

This Transportation Impact Study follows HRM's Guidelines for the Preparation of Transportation Impact Studies, $8^{\text {th }}$ Edition and general traffic and transportation engineering principles for such studies. It is intended to address the transportation impacts that may be expected on the road and active transportation networks resulting from the:

- Removal of the former Scotia Bank building located in the northeast corner of the Wyse Road and Nantucket Avenue; and,
- Addition of a new multi-unit residential / commercial / office development as described in the table below.

Table 1-1:
Project Summary

| Proposed Development | Dunphy Wyse Road Development |
| :--- | :--- |
| Owner | Alex Dunphy |
| Location | Northeast corner of: |
|  | Wyse Road and Nantucket Avenue |
| Building Details | 125 Residential Units |
|  | $9,000 \mathrm{ft}^{2}$ Commercial / Retail Space |
|  | $8,000 \mathrm{ft}^{2}$ Office Space |

Figure 1-1:
Building Rendering


## 2

## Existing Conditions

### 2.1 Study Area

The study area is located in the northeast quadrant of the Wyse Road and Nantucket Avenue intersection, immediately northeast of the Macdonald Bridge in Dartmouth, Nova Scotia. The yellow area represents the new building development site and the blue represents the primary study area considered in this study for analysis purposes.

Figure 2-1: Study Area


### 2.2 Roadways and Intersections

The following sections provide a brief summary of each of the key roadways in the study area that are relevant to this study.


Victoria
Road

Thistle Street

Macdonald Bridge

Victoria Road is the next major roadway north of the development and services traffic between Downtown Dartmouth at its east end and the Circumferential Highway (Hwy 111) at its west end, including its continuation further to the west as Windmill Road. It's intersection with Nantucket Drive is signalized and is a primary route between the Macdonald Bridge and Woodland Avenue / Highway 118. Near Nantucket, Victoria Road includes a westbound dedicated left and shared through/right lane and an eastbound shared through/left with a dedicated right turn channelization and associated approach flare towards the Macdonald Bridge.


Thistle is a two-lane connector roadway between Wyse Road, through Victoria Road and into residential areas to the north of Victoria. It is a common commuter route using Maple Drive as a connection between Thistle and Ochterloney Street. It services the east entry and exit driveways to the Dartmouth Bridge Transit Terminal and includes an access to the Sportplex parking lot. Traffic signals are present at both Victoria Road and Wyse Road.


The Macdonald Bridge is one of the two bridges crossing the Halifax Harbour. The bridge has three lanes with a center reversing lane and is serviced by 5 approach and departure lanes (10 total) as well as bicycle (west side) and pedestrian (east side) lanes on either side of the Bridge. Toll collection includes MacPass technologies and coin collection on all lanes and one attendant is present in each direction for cash transactions.


### 2.3 Active Transportation (AT)

The core downtown areas of both Halifax and Dartmouth have documented high cyclist and pedestrian activity (and other travel modes). This study area is no exception with many local AT origins and destinations surrounding the site and the development has direct access to numerous AT and transit corridors. These include the Dartmouth Bridge Transit Terminal, Dartmouth High and Bicentennial Schools, Dartmouth Common, the recently expanded and renovated Zatzman Sportsplex, Downtown Dartmouth, the Dartmouth waterfront, and various commercial and retail businesses. The development also has direct access to the dedicated bicycle and pedestrian walking lanes that cross the Macdonald Bridge connecting Dartmouth and Halifax.

The majority of routes and intersection crossings are already in place for this development and access points for the development naturally connect to existing sidewalk infrastructure along Nantucket Avenue and Wyse Road.

### 2.4 Vehicle Traffic

Recent and historical traffic counts were provided from HRM for all intersections in the study area. Most counts were completed during 2017 and 2018 and counts were supplemented by transit data, site observations, and general data associated with counts across the Macdonald and MacKay bridges. The baseline counts used in this analysis are provided in Appendix A of this report and the tables in Section 4 of this report show the volumes present on each movement of the intersections under each analysis scenario.

### 2.5 Transit

The proposed development is located immediately southwest of the Dartmouth Bridge Transit Terminal with less than 200 meters between the development and main transit terminal building. The development therefore has direct access to some of the best transit service available in the region with immediate access to over 20 different routes at the terminal and on connecting roadways. Additional routes are available at the Alderney Gate Terminal include the Alderney Ferry to Halifax which is located about 800 meters to the southeast.

### 2.6 Truck Routes



Halifax's By-Law T-400 "Respecting the Establishment of Truck Routes for Certain Trucking Motor Vehicles within the HRM" identifies Wyse Road and Windmill Road as Daytime routes (shown in blue) between the hours of 7 AM and 9 PM. Adjoining "Full Time" truck routes (shown in green) include Albro Lake Road and portions of Victoria Road and Windmill Road to the northwest and the Circumferential Highway via Alderney Drive, Prince Albert or Portland Street. These routes provide direct access to the new development, though limited delivery requirements are expected at this site.


## 3. <br> Future Conditions <br> 3.1 Context

### 3.1.1 Analysis Time Horizon

Based on recommended HRM guidelines, the base year for this study has been established as 2019 and such studies frequently addresses a 5-year time horizon (2024) which includes background traffic growth, new traffic related to the Wyse Road development and any other significant transportation impacts anticipated during that period. Given the relatively low volume of traffic generated by the development relative to the total traffic on the road network, this study addresses the 2019 base year and the 2024 horizon year with the development in place.

### 3.1.2 Background Traffic

Background traffic growth rates for traffic impact studies throughout HRM vary though are often in the $0.5-1 \%$ range. Actual growth is frequently less than this in many areas and even negative in some cases. Much of the natural traffic growth throughout the road network has been influence by the regional planning initiatives implemented over the past decade. Some of this work has resulted in more development closer to the downtown cores of Halifax and Dartmouth. Simultaneously, it has promoted increased transit and active transportation use which in turn has helped limit traffic growth rates for personal vehicles.

To determine reasonable growth rates in past studies for the Dartmouth area, HRM was consulted regarding transportation modeling work that was carried out as part of the regional planning analysis, and those consultations recommended that an average annual growth rate of $0.5 \%$ was appropriate for this general project area. Typically, the background traffic growth rates account for the addition of development throughout the area that contributing to traffic near the development as well as the general impact of trip reductions related to shifts to transit and active transportation modes.

The other important consideration regarding background traffic growth for the purposes of this study is the impact of the Macdonald Bridge, particularly during the peak hours of traffic. The intersection of Wyse Road with Nantucket and the Macdonald Bridge generally operates at, or near capacity during both the AM and PM peak hours. As intersection utilization nears capacity, traffic growth rates typically reduce in favour of the peak period extending over a longer period of time. Given the various factors and inputs, this study has assumed a $0.5 \%$ background traffic growth rate over the 5-year horizon to 2024 and to adjust past studies to the 2019 base year.

### 3.1.3 Analysis Period

Roadways adjacent to the development are highly commuter oriented, particularly given the proximity of the Macdonald Bridge which is a major commuter corridor to between downtown Dartmouth and Halifax. Therefore, the weekday AM and PM peak hours are considered to be the critical periods for the analysis.

### 3.2 The Development

The proposed development is composed primarily of residential units, a relatively small segment of office space, and some ground floor commercial / retail space. To determine a reasonable estimate of trips destined to and from the development during the AM and PM peak hours, the Institute of Transportation Engineers (ITE) Trip Generation Guide (10 ${ }^{\text {th }}$ Edition) was used. The residential portions of the development were represented by "Multifamily Residential Units (high-rise)". The office space assumed the "General Office Building" land use and generated reasonable numbers given the location of the development and access to transit and active transportation infrastructure. The retail component of the space is challenging to define, but it is generally assumed that the nature and the location of the development will not lend itself to a retail use that generates an excessively high volume of new traffic. Frequently, retail space in such developments provide service to local area residents and generate little additional vehicle traffic. For the purposes of this study, the Shopping Center land use was selected as the most reasonable (and conservative) representation of trips to be generated from this development.

The proposed development will require removal of the existing building and construction of the new mixed-use development. As there has been little activity at the existing building in recent years and when operational, the single story building generated relative low traffic volumes, no traffic has been eliminated from the network to account for removal of the building.

### 3.2.1 Trip Generation

The addition of new traffic related to the development is summarized in the table below and a more detailed summary of the trip generation rates, and background calculations are provided in Appendix B of this report. Internal capture rates were estimated using the National Cooperative Highway Research Program (NCHRP) methodologies and no pass-by trips were assumed for the development (i.e. all trips were assigned as new trips to the development).

Table 3-1: Trip Generation Summary

|  | ITE Land | AM Peak |  |  | PM Peak |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Use Type | Enter | Exit | Total | Enter | Exit | Total |
| Multifamily (High Rise) | ITE 222 | 12 | 36 | 48 | 31 | 20 | 51 |
| Office | ITE 710 | 8 | 1 | 9 | 1 | 8 | 9 |
| Misc. Retail | ITE 820 | 5 | 3 | 8 | 16 | 18 | 34 |
| Internal Capture Trips | (NCHRP) | 0 | 0 | 0 | -9 | -9 | -18 |
| TOTAL |  | $\mathbf{2 5}$ | $\mathbf{4 0}$ | $\mathbf{6 5}$ | $\mathbf{3 9}$ | $\mathbf{3 7}$ | $\mathbf{7 6}$ |

Given the proximity to Bridge transit hub and access to the robust active transportation network, it is expected that the development will generate traffic at rates significantly less than those estimated for "typical" mixed use developments. In the case of this development, trip reduction is expected to impact both origin related traffic (i.e. residents traveling from the development to work) as well as destination-based trips (i.e. people traveling to the office or retail portions of the development). In addition, the development is at a location that should incentivize the use of alternate modes of travel given the congestion frequently experienced on the Macdonald Bridge. Nonetheless, no additional trip reduction factors were assumed for the purposes of this study.

### 3.3 Trip Distribution and Assignment

It is assumed that traffic will distribute itself through the network in a similar manner to the existing traffic. The new building will have a mix of inbound peak traffic and outbound peak traffic (i.e. primarily inbound office traffic and outbound residential traffic in the AM peak).

### 3.3.1 Driveway Location

The location for the development's driveway access to the underground parking structure has been discussed extensively and various options have been proposed. The original and preferred location from a traffic operations and safety perspective was to locate the driveway at the northeast corner of the development connecting to the main circulation aisle through the Sportsplex parking lot. This location corresponded with one of the existing driveways to the former Scotiabank surface parking lot, thought HRM informed the developer that any access off the Sportsplex parking lot would not be permitted.

This resulted in the evaluation of alternative access locations which identified one option off Nantucket Avenue and one option off Wyse Road. Both alternative access points would require some level of turn restrictions to function effectively which is discussed in greater detail in the conclusions section of this report. A preliminary analysis of the Wyse Road and Nantucket Avenue driveway options shows that there is very little difference on the impacts to network traffic operations between the two options. Therefore, for the purposes of this study, we have analyzed the network using the Nantucket Road intersection only and further assumed that this intersection would function as a right-in, right-out only access.

Regardless of the access driveway, adjacent intersections can experience some level of congestion related to access to the Macdonald Bridge. It is therefore anticipated that entry and exit movements from the development may vary day-to-day depending on the level of congestion on the adjacent roadways. It is also anticipated that congestion may result in some drivers electing to use alternate routes to get between the development and their intended external origin or destination. The trip assignment assumptions and results are reflected in the spreadsheets and tables included in Appendix C of this report.

## 4 Analysis

### 4.1 Transportation Modelling

A microscopic traffic model was prepared using the Synchro/SimTraffic platform for the AM and PM peak hours of analysis. Detailed output for each of the scenarios is provided in Appendix D of the report. The analysis included the following models for each of the AM and PM peaks:

- 2019 existing conditions;
- 2024 conditions with background traffic only; and,
- 2024 with background and development traffic.

The trip assignment process suggested that traffic entering and exiting the development on Nantucket Avenue will have to use circuitous routes in some cases to get to or from the driveway. For example, a driver approaching the site from the northwest (say from Dartmouth Crossing), will likely use Boland Street to Wyse Road then turn left onto Nantucket to enter the driveway because a left turn is not permitted from Nantucket to the driveway. This study assumes that all drivers remain on the main road network and use the most convenient route between the driveway and their external origin or destination, though it is possible some drivers may elect to use various shortcut or U-turn options to shorten their routes.

In general, intersections in the study area operate at a reasonably good level of service with limited delays and queues, while the intersection of Wyse Road with the Macdonald Bridge and Nantucket can experience frequent congestion during the peak hours. The individual intersections most impacted by the development are discussed in greater detail in the following sections and detailed results for all intersections for each analysis scenario are provided in Appendix D of this report.

### 4.2 Development Driveway

The development's driveway was assumed to operate as a right-in, right-out only access. The traffic signals at the Wyse Road intersection immediately to the south combined with the limited eastbound left turn volumes from Wyse to Nantucket and three-lane cross section adjacent to the driveway result in significant gaps in traffic allowing the driveway movements to operate at a high level of service. Modeling results show that in the worst case, the driveway intersection operates with a volume to capacity ratio of 0.25 or less, delays less than 10 seconds and minimal queuing. Detailed results are provided for the 2024 Development scenarios only (driveway is not present in existing and background traffic only scenarios) in Appendix D of this report for intersection \#18: Nantucket and Driveway.

### 4.3 Nantucket Ave/Sportsplex/Mall Driveway

This is the first intersection immediately north of the site and accommodates all traffic exiting the site if the development's driveway is located on Nantucket Street. Conversely, all traffic entering the site will come from the south and will not travel through this intersection. The Nantucket driveway option therefore represents the worst-case scenario for traffic operations as volumes at this intersection will would be lower if the driveway were located on Wyse Road. This intersection includes pedestrian actuated traffic signals on the north side of the intersection. The majority of green time remains attributed to through movements on Nantucket Avenue to service volumes coming off the Macdonald Bridge. This intersection is located at an adequate distance from the proposed driveway to meet the minimum 30 meter separation distance suggested by HRM by-laws.

The Synchro modeling results suggest that the AM peak experiences maximum volume to capacity ratio's of about 0.50 ( $50 \%$ capacity) today and 0.51 under 2024 development conditions with an overall intersection capacity utilization of about $53 \%$. There is little change in operational results between existing and future development conditions during AM or PM peak hours. The two figures below present the volumes, volume to capacity ratio's and average vehicle delays for each movement at the intersection during the AM and PM peak hours.

| AM Peak |  | Mall Driveway |  |  | Sportsplex |  |  | Nantucket NB |  |  | Nantucket SB |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | EBL |  |  |  |  |  |  |  |  | ${ }_{S B L}$ |  |  |
|  |  | $4{ }^{4}$ |  | NT1 |  |  | tits |  |  |
|  | Vol |  |  |  |  | 5 | 3 | 4 | 39 | 24 | 280 | 44 | 20 | 939 | 59 |
|  | V/C |  |  | 0.01 | 0.12 |  |  | 0.16 |  | 0.04 | 0.50 |  |  |
|  | Delay |  |  | 0.0 | 14.2 |  |  | 5.7 |  | 1.7 | 8.1 |  |  |
| No | Vol |  |  | 5 | 3 | 4 | 40 | 25 | 287 | 45 | 21 | 963 | 60 |
|  | V/C |  |  | 0.01 | 0.12 |  |  | 0.17 |  | 0.05 | 0.51 |  |  |
|  | Delay |  |  | 0.0 | 14.2 |  |  | 5.7 |  | 1.7 | 8.2 |  |  |
|  | Vol |  |  | 5 | 3 | 4 | 40 | 25 | 326 | 47 | 21 | 963 | 60 |
|  | V/C |  |  | 0.01 | 0.12 |  |  | 0.19 |  | 0.05 | 0.51 |  |  |
| - | Delay |  |  | 0.0 | 14.2 |  |  | 5.8 |  | 1.7 | 8.2 |  |  |



In general, this intersection operates at a high level of performance throughout all scenarios and given the robust nature of the adjacent road network, no specific improvements are required at this intersection to accommodate the development. Modelling results suggest that there may be some benefits achieved for operations on Nantucket with improved coordination between the signals at the Sportsplex Driveway and signals at Wyse Road with Nantucket.

### 4.4 Nantucket Ave. / Victoria Rd. / School St.

The second signalized intersection to the north of the site has very limited impact from development-based traffic which composes about $2 \%$ of the overall traffic at the intersection in the 2024 development scenario. The heaviest movements during the AM peak hour are the eastbound right turn and westbound left turn from Victoria to Nantucket and the modelling results suggest an overall intersection capacity utilization of about $73 \%$ with volume to capacity ratios remaining less than 0.60 on all movements.

PM peak traffic is impacted by the heavier volume of northbound traffic on Nantucket making a left turn onto Victoria Road resulting in a movement $\mathrm{v} / \mathrm{c}$ ratio of around 0.95 and some substantial queuing. That said, the queuing is not unreasonable given the heavy volume of traffic crossing the Macdonald Bridge during peak hour operations and there is available capacity on other movements at the intersection that could allow a more even distribution of capacity utilization if desired. Opposing traffic on School Road is relatively low so the northbound left turn movement generally operates with limited delay. Overall capacity utilization is around $77 \%$ at this intersection.

| AM Peak |  | Victoria Road |  |  | Victoria Road |  |  | Nantucket Avenue |  |  | School Street |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | 4 |  |  | - 1 |  |  | Fi |  |  | 4 |  |  |
| No | Vol | 10 | 80 | 510 | 330 | 300 | 27 | 165 | 45 | 109 | 20 | 180 | 10 |
|  | V/C | 0.11 |  | 0.53 | 0.57 | 0.39 |  | 0.45 | 0.25 |  | 0.36 |  |  |
|  | Delay | 19.3 |  | 14.3 | 15.5 | 11.0 |  | 19.7 | 6.2 |  | 16.0 |  |  |
| İ | Vol | 10 | 82 | 523 | 338 | 308 | 28 | 169 | 46 | 112 | 21 | 185 | 10 |
|  | V/C | 0.11 |  | 0.54 | 0.58 | 0.40 |  | 0.47 | 0.26 |  | 0.37 |  |  |
|  | Delay | 19.3 |  | 14.5 | 15.5 | 11.0 |  | 19.7 | 6.2 |  | 16.0 |  |  |
|  | Vol | 10 | 82 | 523 | 338 | 308 | 28 | 198 | 48 | 120 | 22 | 185 | 10 |
|  | V/C | 0.11 |  | 0.54 | 0.58 | 0.40 |  | 0.55 | 0.27 |  | 0.37 |  |  |
|  | Delay | 19.3 |  | 14.5 | 15.5 | 11.0 |  | 21.8 | 6.1 |  | 16.0 |  |  |


| PM <br> Peak |  | Victoria Road |  |  | Victoria Road |  |  | Nantucket Avenue |  |  | School Street |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | A |  |  | 1 1 |  |  | $\cdots$ |  |  | 4 |  |  |
| \| | Vol | 20 | 209 | 368 | 134 | 199 | 50 | 577 | 65 | 169 | 20 | 48 | 10 |
|  | V／C | 0.46 |  | 0.58 | 0.49 | 0.48 |  | 0.87 | 0.26 |  | 0.09 |  |  |
|  | Delay | 32.9 |  | 21.9 | 24.0 | 19.2 |  | 28.6 | 3.0 |  | 6.1 |  |  |
|  | Vol | 21 | 214 | 377 | 137 | 204 | 51 | 592 | 67 | 173 | 21 | 49 | 10 |
|  | V／C | 0.46 |  | 0.58 | 0.49 | 0.48 |  | 0.87 | 0.26 |  | 0.09 |  |  |
|  | Delay | 32.9 |  | 21.9 | 24.0 | 19.2 |  | 28.6 | 3.0 |  | 6.1 |  |  |
| NiN⿳亠二口欠刂 | Vol | 21 | 214 | 377 | 137 | 204 | 51 | 621 | 68 | 179 | 23 | 49 | 10 |
|  | V／C | 0.48 |  | 0.59 | 0.51 | 0.50 |  | 0.95 | 0.27 |  | 0.10 |  |  |
|  | Delay | 32.9 |  | 22.2 | 24.8 | 19.5 |  | 39.2 | 3.0 |  | 6.2 |  |  |

## 4．5 Wyse Rd／Macdonald Bridge／Nantucket

This intersection is one of the highest volume intersections in HRM and is characterized by eastbound double right，westbound double left，southbound double through lanes on the approaches．Operations vary significantly day－to－day depending on the peak traffic characteristics that are often dependent on driver choices on the approaching road network．The AM peak hour frequently experiences some congestion as vehicles enter onto the Macdonald Bridge from all three approaches．

Queues frequently extend across the Macdonald Bridge from the Halifax side of the Harbour which contributes to congestion at this intersection．Exacerbating the challenges are the left turn bus movements from the westbound dedicated bus lane on Wyse Road onto the Macdonald Bridge which frequently blocks the eastbound right turn movements onto the Bridge from Wyse Road．

For all these reasons，this is a difficult intersection to accurately model．The modelling result suggest that in the absence of backups on the Macdonald Bridge（from the Halifax side）that limit the efficiency of the intersection，the intersection operates with an overall capacity utilization of about $82 \%$ in the AM and PM peaks．During these periods，movements to the Bridge frequently operate with a V／C ratio over 0.9 and substantial queuing can occur．Often，one or two of the three approach legs run at capacity and observations in the area suggest that some drivers will seek alternate routes to less congested approaches．

| AM Peak |  | Wyse（EB） |  |  | Wyse（WB） |  |  | Macdonald Brdg |  |  | Nantucket |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | 「＂ |  |  |  |  |  |  |  |  |  |
| ain | Vol | 66 | 100 | 665 | 803 | 83 | 28 | 143 | 254 | 485 | 0 | 903 | 8 |
|  | V／C | 0.26 | 0.27 | 0.74 | 0.90 |  |  | 0.70 | 0.12 | 0.51 |  | 0.83 |  |
|  | Delay | 33.5 | 32.7 | 33.4 | 47.8 |  |  | 37.8 | 16.5 | 3.8 |  | 37.0 |  |
|  | Vol | 68 | 103 | 682 | 823 | 85 | 29 | 147 | 260 | 497 | 0 | 926 | 8 |
|  | V／C | 0.26 | 0.28 | 0.76 | 0.92 |  |  | 0.72 | 0.12 | 0.52 |  | 0.85 |  |
|  | Delay | 33.6 | 32.9 | 34.2 | 49.8 |  |  | 39.8 | 16.5 | 3.9 |  | 38.6 |  |
|  | Vol | 76 | 103 | 698 | 823 | 85 | 35 | 147 | 271 | 497 |  | 926 | 8 |
|  | V／C | 0.29 | 0.28 | 0.78 | 0.92 |  |  | 0.72 | 0.13 | 0.52 |  | 0.85 |  |
|  | Delay | 34.3 | 32.8 | 35.0 | 49.9 |  |  | 40.0 | 16.6 | 3.9 |  | 38.8 |  |

Various signal timing adjustments can be made during the AM peak hours to distribute capacity and queuing through the intersection，though all have very limited impact on the overall operations at the intersection．Given the nature of the intersection as the entrance to the Macdonald Bridge，it is expected that there will always be some level of congestion for movements approaching the bridge．As the development based volumes are so low，there is virtually no change to performance measures with the development traffic added．

| PM Peak |  | Wyse（EB） |  |  | Wyse（WB） |  |  | Macdonald Bridge |  |  | Nantucket |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | 7＇7 |  |  |  |  |  |  |  |  |  |
|  | Vol | 60 | 128 | 375 | 447 | 142 | 50 | 283 | 654 | 1011 |  | 543 | 22 |
|  | V／C | 0.29 | 0.41 | 0.39 | 0.66 | 0.26 |  | 0.70 | 0.26 | 0.85 |  | 0.48 |  |
|  | Delay | 34.4 | 34.9 | 22.5 | 36.4 | 14.4 |  | 26.6 | 13.6 | 13.0 |  | 25.0 |  |
| 菏咅品亳 | Vol | 62 | 131 | 384 | 458 | 146 | 51 | 290 | 671 | 1037 |  | 557 | 23 |
|  | V／C | 0.29 | 0.41 | 0.39 | 0.66 | 0.26 |  | 0.70 | 0.26 | 0.85 |  | 0.48 |  |
|  | Delay | 39.0 | 41.7 | 13.9 | 47.0 | 19.7 |  | 20.1 | 10.7 | 16.2 |  | 20.8 |  |
|  | Vol | 74 | 131 | 400 | 458 | 146 | 64 | 290 | 687 | 1037 |  | 557 | 23 |
|  | V／C | 0.36 | 0.41 | 0.41 | 0.67 | 0.28 |  | 0.75 | 0.28 | 0.87 |  | 0.50 |  |
|  | Delay | 36.0 | 34.8 | 22.8 | 36.9 | 14.2 |  | 29.7 | 14.0 | 15.3 |  | 25.5 |  |

PM peak operations at this intersection are slightly better than during the AM peak hour as level of service through the intersection is heavily dictated by the ability to get vehicles through the Macdonald Bridge toll plaza and then through the signals at Wyse Road．The available capacity of the signals typically causes queueing to extend across the bridge toward the Halifax side and limits the amount of traffic downstream of the intersection．With respect to the impacts of the development，the new traffic composes well less the $1 \%$ of the total traffic through the intersection and therefore does not generate any specific recommendations for improvements at this intersection．

### 4.6 Wyse Road and Thistle Street

This is the first intersection east of the proposed development and like other intersections in the study area, development traffic has minimal impact on the intersection's operations. Development traffic composes about 1\% of total traffic through the intersection during the peak hours. V/C ratios and overall intersection capacity utilization remain below $50 \%$ during the AM peak hour with limited delay and queuing. During the PM peak the heavier eastbound left to Thistle competes with the westbound through movement on Wyse resulting in $\mathrm{v} / \mathrm{c}$ ratios of about 0.9 , though the traffic signals help keep delays and queue lengths at reasonable levels.

| AM Peak |  | Wyse (EB) |  | Wyse (WB) |  | Thistle |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{aligned} & *- \\ & \text { WBT } \end{aligned}$ |  |  | $\begin{aligned} & 4 \\ & \hline \operatorname{SBR} \end{aligned}$ |
|  |  | \% 14 |  | 中 ${ }^{\text {a }}$ |  | \% ${ }^{\text {T }}$ |  |
| $\underset{\sim}{\sim} \underset{\sim}{\stackrel{\rightharpoonup}{x}}$ | Vol | 88 | 497 | 565 | 41 | 57 | 349 |
|  | V/C | 0.56 | 0.50 | 0.61 |  | 0.07 | 0.43 |
|  | Delay | 27.1 | 15.2 | 16.4 |  | 8.0 | 6.5 |
|  | Vol | 90 | 510 | 579 | 42 | 58 | 358 |
|  | V/C | 0.57 | 0.50 | 0.61 |  | 0.07 | 0.44 |
|  | Delay | 28.0 | 15.2 | 16.3 |  | 8.2 | 7.1 |
|  | Vol | 90 | 510 | 583 | 42 | 65 | 361 |
|  | V/C | 0.58 | 0.50 | 0.62 |  | 0.08 | 0.45 |
|  | Delay | 28.3 | 15.2 | 16.4 |  | 8.2 | 7.2 |


| PM <br> Peak |  | Wyse (EB) |  | Wyse (WB) |  | Thistle |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{array}{ll} 4 & 4 \\ \text { WBT } & \text { WBR } \end{array}$ |  |  |  |
|  |  | * 14 |  |  |  | ${ }^{7}$ |  |
|  | Vol | 362 | 687 | 671 | 62 | 70 | 172 |
|  | V/C | 0.89 | 0.39 | 0.79 |  | 0.14 | 0.30 |
|  | Delay | 37.0 | 8.6 | 25.6 |  | 16.2 | 4.6 |
|  | Vol | 371 | 704 | 688 | 64 | 72 | 176 |
|  | V/C | 0.89 | 0.39 | 0.79 |  | 0.14 | 0.30 |
|  | Delay | 37.0 | 8.6 | 25.6 |  | 16.2 | 4.6 |
|  | Vol | 371 | 704 | 694 | 64 | 79 | 182 |
|  | V/C | 0.92 | 0.40 | 0.81 |  | 0.16 | 0.32 |
|  | Delay | 41.6 | 8.6 | 26.7 |  | 16.5 | 4.6 |

### 4.7 Development Driveway Location

The originally proposed driveway location from the Sportsplex parking lot was not permitted. Therefore, alternative driveway options on Nantucket Avenue and Wyse Road were evaluated and summarized in a March 2020 letter that addressed the adjacent roadway environment, and operational and safety implications of each driveway option. The letter is attached in Appendix E for reference with the key findings summarized in the points below:

- Both driveway options are feasible and meet the 30-meter minimum required separation from the nearest street line of the Wyse/Nantucket/Macdonald Bridge intersection;
- Driveway volumes are low which minimize the driveway's impacts on adjacent traffic;
- Due to the proximity of the intersection and the adjacent lanes / operations, both driveway options should be configured as right-in, right-out driveways. Comments provided by HRM suggest that supplementary measures may be required to limit the possibility of making left turn movements. Further discussion should take place as the project moves into detailed design stages and options could include directional islands and the extension of medians;
- Both driveway options introduce some level of route restrictions between the development and external origins / destinations. The specific route challenges associated with each driveway option are detailed in the attached letter, though it is difficult to predict exactly how drivers will respond to various traffic conditions. Suffice to say that the surrounding road network is robust and there are a wide variety of alternative routing options that remain relatively short and convenient;
- Comments from Halifax Transit suggest that the Nantucket driveway option appears to minimize the potential impacts to transit operations and is therefore preferred;
- Comments from HRM have indicated that detailed design work is proceeding on unidirectional protected bicycle lanes on Wyse Road, between Boland Road and Thistle St. with construction expected to begin in 2020.

Based on the various analyses and feedback comments, it appears that there is a collective preference to pursue the Nantucket Road driveway option. Under this scenario, the preferred driveway location should maximize the distance away from the Wyse Road intersection while not compromising spacing to the Sportsplex driveway or the ability to achieve appropriate grading to the development's parking structure. At the current time, the preferred location appears to be approximately at the midpoint between Wyse Road and the Sportsplex driveway. This results in about 40 meters between the driveway and each of the adjacent intersections.

Given the complex environment and interests of various HRM departments, further refinement of the driveway location and operational characteristics should be discussed as part of the detailed design process and subsequent to this transportation impact study.

## 5. Conclusions

This report has analyzed the impacts of the removal of an existing building and the addition of a new multi-unit residential development with office and retail space. The analysis shows that the development contributes a very small amount of traffic to the adjacent roadways and intersections relative to the overall traffic on the road network. Furthermore, the results show very little change to key performance parameters such as delays, queue length or volume to capacity ratios between conditions before and after the development is in place.

The surrounding road network is characterized by high volumes of commuter-based traffic, most notably related to volumes onto and off the Macdonald Bridge between Dartmouth and Halifax. This commuter traffic is quite consistent during the weekdays, though the intensity of traffic on the three directional approaches to the Bridge can vary significantly. In general, the development fits very well into the surrounding environment being directly located on several core transportation routes and having direct access to robust transit and active transportation networks. It is expected that residents of this development are highly likely to utilize both the transit and AT networks which in turn help to reduce additional vehicle traffic on the roadways.

The analysis suggests that there are no improvements required to the external road network to accommodate the proposed development. Analysis and HRM feedback suggests that the preferred location of the site's parkade driveway is off Nantucket Avenue approximately 40 meters north of Wyse Road. Refinement of the driveway's location and geometrics should be undertaken in conjunction with HRM as the project moves into the detailed design stages.

We trust that this report satisfies the Halifax requirements for the preparation of Transportation Impact Studies. Should there be any questions or comments regarding the content of the study, please do not hesitate to contact the undersigned.

Sincerely,
Original Signed


Roger N. Boychuk, P.Eng.
Senior Transportation Engineer


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1 Starr Lane, Dartmouth, NS B2Y 4V7
c: (902) 2331152
www.fathomstudio.ca


## APPENDIX A

## Traffic Counts

HALIFAX REGIONAL MUNICIPALITY

## MANUAL TRAFFIC COUNTS



TOTAL
PEAK
15 MIN PEAK
PEAK HOUR FACTOR
TWO WAY TOTALS

| 20 | 930 | 58 | 0 | 268 | 32 | 0 | 0 | 2 | 3 | 4 | 39 | 1356 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1008 |  |  | 300 |  |  | 2 |  |  | 46 |  |  |
|  | 1100 |  |  | 372 |  |  | 8 |  |  | 60 |  |  |
|  | 0.92 |  |  | 0.81 |  |  | 0.25 |  |  | 0.77 |  |  |
|  | 1315 |  |  | 1235 |  |  | 64 |  |  | 98 |  | FACTOR |
|  |  |  |  |  |  |  |  |  |  |  |  | 1.01 |
|  |  |  |  |  |  |  |  |  |  |  |  | 1370 |


| DAY | DATE | MONTH | YEAR |
| :---: | :---: | :---: | :---: |
| TUES | 7 | NOV | 2017 |


| TIME: <br> 15 MIN INTERVALS |  | FROM THE EAST |  |  | FROM THE WEST |  |  | FROM THE NORTH |  |  | FROM THE SOUTH |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | L | S | R | L | S | R | L | S | R | L | S | R |  |
| 08:00:00 AM | 08:15:00 AM | 2 | 197 | 13 | 0 | 65 | 4 | 0 | 0 | 0 | 1 | 1 | 1 | 284 |
| 08:15:00 AM | 08:30:00 AM | 4 | 223 | 12 | 1 | 79 | 2 | 0 | 0 | 0 | 0 | 2 | 5 | 328 |
| 08:30:00 AM | 08:45:00 AM | 2 | 204 | 14 | 0 | 71 | 3 | 0 | 0 | 0 | 1 | 0 | 3 | 298 |
| 08:45:00 AM | 09:00:00 AM | 5 | 218 | 12 | 0 | 65 | 3 | 0 | 0 | 0 | 1 | 2 | 2 | 308 |


| TOTAL | 13 | 842 | 51 | 1 | 280 | 12 | 0 | 0 | 0 | 3 | 5 | 11 | 1218 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PEAK |  | 906 |  |  | 293 |  |  | 0 |  |  | 19 |  |  |
| 15 MIN PEAK |  | 956 |  |  | 328 |  |  | 0 |  |  | 28 |  |  |
| PEAK HOUR FACTOR |  | 0.95 |  |  | 0.89 |  |  | 0 |  |  | 0.68 |  |  |
| TWO WAY TOTALS |  | 1197 |  |  | 1138 |  |  | 57 |  |  | 44 |  | FACTOR |
|  |  |  |  |  |  |  |  |  |  |  |  |  | 1.01 |
|  |  |  |  |  |  |  |  |  |  |  |  |  | 1230 |

VEHICULAR GRAPHIC SUMMARY SHEET
INTERSECTION :



HALIFAX REGIONAL MUNICIPALITY

## MANUAL TRAFFIC COUNTS

| INTERSECTIO |  |  |  |  | UC | AVEN | T D | U | OR |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  | $\overline{A T}$ |  |  | JDY |
| DAY | DATE | MONTH | YEAR |  |  |  |  |  |  |  | CO |  |  |  |
| TUES | 7 | NOV | 2017 |  |  |  |  |  |  |  |  |  |  |  |
| STREET: |  | NANTU | CKET | NUE |  | KEET | NUE |  | MAL |  | RT | S | SPL |  |
| TIME: |  | FRO | M THE |  |  | THE |  |  | HE |  |  | HE |  | TOTAL |
| 15 MIN INTER | VALS | L | S | R | L | S | R | L | S | R | L | S | R |  |
| 04:00:00 PM | 04:15:00 PM | 0 | 92 | 19 | 0 | 183 | 3 | 0 | 0 | 3 | 0 | 0 | 8 | 308 |
| 04:15:00 PM | 04:30:00 PM | 1 | 98 | 9 | 0 | 197 | 1 | 0 | 0 | 3 | 0 | 0 | 8 | 317 |
| 04:30:00 PM | 04:45:00 PM | 0 | 103 | 16 | 0 | 201 | 2 | 0 | 0 | 4 | 1 | 0 | 13 | 340 |
| 04:45:00 PM | 05:00:00 PM | 0 | 108 | 22 | 1 | 200 | 2 | 0 | 0 | 2 | 0 | 0 | 12 | 347 |


| TOTAL | 1 | 401 | 66 | 1 | 781 | 8 | 0 | 0 | 12 | 1 | 0 | 41 | 1312 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PEAK |  | 468 |  |  | 790 |  |  | 12 |  |  | 42 |  |  |
| 15 MIN PEAK |  | 520 |  |  | 812 |  |  | 16 |  |  | 56 |  |  |
| PEAK HOUR FACTOR |  | 0.9 |  |  | 0.97 |  |  | 0.75 |  |  | 0.75 |  |  |
| TWO WAY TOTALS |  | 1290 |  |  | 1204 |  |  | 79 |  |  | 51 |  | FACTOR |
|  |  |  |  |  |  |  |  |  |  |  |  |  | 1.01 |
|  |  |  |  |  |  |  |  |  |  |  |  |  | 1325 |



| TOTAL | 1 | 451 | 74 | 1 | 791 | 11 | 0 | 0 | 7 | 5 | 0 | 24 | 1365 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PEAK |  | 526 |  |  | 803 |  |  | 7 |  |  | 29 |  |  |
| 15 MIN PEAK |  | 568 |  |  | 872 |  |  | 12 |  |  | 52 |  |  |
| PEAK HOUR FACTOR |  | 0.93 |  |  | 0.92 |  |  | 0.58 |  |  | 0.56 |  |  |
| TWO WAY TOTALS |  | 1341 |  |  | 1266 |  |  | 82 |  |  | 41 |  | FACTOR |
|  |  |  |  |  |  |  |  |  |  |  |  |  | 1.01 |
|  |  |  |  |  |  |  |  |  |  |  |  |  | 1379 |

VEHICULAR GRAPHIC SUMMARY SHEET
INTERSECTION :



HALIFAX REGIONAL MUNICIPALITY
TRANSPORTATION \& PUBLIC WORKS
CODE NO.
17-TM-311
TRAFFIC \& RIGHT OF WAY

## MANUAL TRAFFIC COUNTS

| INTERSECTIO |  |  |  |  |  | LE S | T | OR | AD |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  | EAT |  |  |  |
| DAY | DATE | MONTH | YEAR |  |  |  |  |  |  |  | CO |  |  |  |
| TUESDAY | 17 | OCT | 2017 |  |  |  |  |  |  |  |  |  |  |  |
| STREET: |  | THIS | TLE S |  |  | LE S |  |  | IA |  |  | RIA |  |  |
| TIME: |  | FRO | M THE |  |  | THE |  |  | HE |  |  | THE |  | TOTAL |
| 15 MIN INTER | VALS | L | S | R | L | S | R | L | S | R | L | S | R |  |
| 07:00:00 AM | 07:15:00 AM | 0 | 59 | 69 | 2 | 20 | 2 | 12 | 18 | 12 | 19 | 92 | 0 | 305 |
| 07:15:00 AM | 07:30:00 AM | 0 | 73 | 64 | 8 | 25 | 1 | 13 | 10 | 12 | 17 | 89 | 0 | 312 |
| 07:30:00 AM | 07:45:00 AM | 1 | 66 | 56 | 8 | 22 | 1 | 12 | 12 | 14 | 25 | 107 | 1 | 325 |
| 07:45:00 AM | 08:00:00 AM | 2 | 79 | 60 | 12 | 26 | 1 | 15 | 18 | 13 | 23 | 85 | 0 | 334 |

TOTAL
PEAK
15 MIN PEAK
PEAK HOUR FACTOR
TWO WAY TOTALS

| 3 | 277 | 249 | 30 | 93 | 5 | 52 | 58 | 51 | 84 | 373 | 1 |
| :--- | :--- | :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 529 |  |  | 128 |  |  | 161 |  | 458 |  |  |
|  | 564 |  | 156 |  |  | 184 |  | 532 |  |  |  |
|  | 0.94 |  |  |  | 0.88 |  | 0.86 |  |  |  |  |
|  | 675 |  | 540 |  | 813 | 524 |  |  |  |  |  |
|  |  |  |  |  | 1.01 |  |  |  |  |  |  |


| DAY | DATE | MONTH | YEAR |
| :---: | :---: | :---: | :---: |
| TUESDAY | 17 | OCT | 2017 |


| TIME: <br> 15 MIN INTERVALS |  | FROM THE EAST |  |  | FROM THE WEST |  |  | FROM THE NORTH |  |  | FROM THE SOUTH |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | L | S | R | L | S | R | L | S | R | L | S | R |  |
| 08:00:00 AM | 08:15:00 AM | 2 | 48 | 48 | 22 | 18 | 3 | 19 | 28 | 15 | 12 | 74 | 1 | 290 |
| 08:15:00 AM | 08:30:00 AM | 3 | 72 | 58 | 23 | 23 | 5 | 19 | 29 | 19 | 10 | 62 | 1 | 324 |
| 08:30:00 AM | 08:45:00 AM | 15 | 75 | 55 | 13 | 58 | 5 | 17 | 24 | 14 | 2 | 43 | 1 | 322 |
| 08:45:00 AM | 09:00:00 AM | 21 | 61 | 59 | 11 | 42 | 2 | 22 | 31 | 14 | 20 | 46 | 0 | 329 |


| TOTAL | 41 | 256 | 220 | 69 | 141 | 15 | 77 | 112 | 62 | 44 | 225 | 3 | 1265 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PEAK | 517 |  |  | 225 |  |  | 251 |  |  | 272 |  |  |  |
| 15 MIN PEAK | 580 |  |  | 304 |  |  | 268 |  |  | 348 |  |  |  |
| PEAK HOUR FACTOR | 0.89 |  |  | 0.74 |  |  | 0.94 |  |  | 0.78 |  |  |  |
| TWO WAY TOTALS | 738 |  |  | 587 |  |  | 765 |  |  | 440 |  |  | FACTOR |
|  |  |  |  |  |  |  |  |  |  |  |  |  | 1.01 |
|  |  |  |  |  |  |  |  |  |  |  |  |  | 1278 |



HALIFAX REGIONAL MUNICIPALITY
TRANSPORTATION \& PUBLIC WORKS
CODE NO.
17-TM-311
TRAFFIC \& RIGHT OF WAY

## MANUAL TRAFFIC COUNTS

| INTERSECTION: |  | THISTLE STREET AT VICTORIA ROAD |  |
| :---: | :---: | :---: | :---: |
|  |  |  |  |
| DAY | DATE | MONTH | YEAR |
| TUESDAY | 17 | OCT | 2017 |


| STREET: |  |  | E S |  |  | LE S |  |  | IA S |  |  | IA |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TIME: |  |  | THE |  |  | THE |  |  | HE |  |  | THE |  | TOTAL |
| 15 MIN INTER | VALS | L | S | R | L | S | R | L | S | R | L | S | R |  |
| 04:00:00 PM | 04:15:00 PM | 1 | 21 | 21 | 11 | 124 | 4 | 50 | 19 | 8 | 5 | 47 | 2 | 313 |
| 04:15:00 PM | 04:30:00 PM | 3 | 38 | 40 | 9 | 143 | 3 | 69 | 39 | 8 | 6 | 58 | 3 | 419 |
| 04:30:00 PM | 04:45:00 PM | 0 | 24 | 25 | 10 | 111 | 6 | 59 | 25 | 11 | 12 | 77 | 3 | 363 |
| 04:45:00 PM | 05:00:00 PM | 1 | 32 | 35 | 7 | 117 | 2 | 66 | 24 | 21 | 14 | 45 | 0 | 364 |

TOTAL
PEAK
15 MIN PEAK
PEAK HOUR FACTOR
TWO WAY TOTALS

| 5 | 115 | 121 | 37 | 495 | 15 | 244 | 107 | 48 | 37 | 227 | 8 | 1459 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 241 |  |  | 547 |  |  | 399 |  |  | 272 |  |  |  |
| 324 |  |  | 620 |  |  | 464 |  |  | 368 |  |  |  |
| 0.74 |  |  | 0.88 |  |  | 0.86 |  |  | 0.74 |  |  |  |
| 988 |  |  | 747 |  |  | 784 |  |  | 399 |  |  | FACTOR |
|  |  |  |  |  |  |  |  |  |  |  |  | 1.01 |
|  |  |  |  |  |  |  |  |  |  |  |  | 1474 |


| DAY | DATE | MONTH | YEAR |
| :---: | :---: | :---: | :---: |
| TUESDAY | 17 | OCT | 2017 |


| TIME: <br> 15 MIN INTERVALS |  | FROM THE EAST |  |  | FROM THE WEST |  |  | FROM THE NORTH |  |  | FROM THE SOUTH |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | L | S | R | L | S | R | L | S | R | L | S | R |  |
| 05:00:00 PM | 05:15:00 PM | 0 | 38 | 26 | 8 | 116 | 4 | 64 | 34 | 17 | 11 | 78 | 1 | 397 |
| 05:15:00 PM | 05:30:00 PM | 2 | 45 | 25 | 8 | 123 | 9 | 56 | 9 | 9 | 7 | 45 | 0 | 338 |
| 05:30:00 PM | 05:45:00 PM | 1 | 32 | 28 | 7 | 112 | 7 | 56 | 29 | 18 | 6 | 36 | 1 | 333 |
| 05:45:00 PM | 06:00:00 PM | 0 | 29 | 38 | 9 | 117 | 7 | 57 | 20 | 19 | 4 | 46 | 0 | 346 |


| TOTAL | 3 | 144 | 117 | 32 | 468 | 27 | 233 | 92 | 63 | 28 | 205 | 2 | 1414 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PEAK |  | 264 |  |  | 527 |  |  | 388 |  |  | 235 |  |  |
| 15 MIN PEAK |  | 288 |  |  | 560 |  |  | 460 |  |  | 360 |  |  |
| PEAK HOUR FACTOR |  | 0.92 |  |  | 0.94 |  |  | 0.84 |  |  | 0.65 |  |  |
| TWO WAY TOTALS |  | 967 |  |  | 762 |  |  | 742 |  |  | 357 |  | FACTOR |
|  |  |  |  |  |  |  |  |  |  |  |  |  | 1.01 |
|  |  |  |  |  |  |  |  |  |  |  |  |  | 1428 |



## MANUAL TRAFFIC COUNTS




## MANUAL TRAFFIC COUNTS

| INTERSECTION: |  | BOLAND ROAD AT WYSE ROAD |  |  |  |  |  |  | WEATHER RECORDER |  |  | SUNNY / CLEAR |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DAY | DATE | MONTH | YEAR |  |  |  |  |  |  |  |  |  |  |  |
| WED | 7 | SEPT | 2016 |  |  |  |  |  |  |  |  |  |  |  |
| STREET: <br> TIME: <br> 15 MIN INTERVALS |  | BOLAND ROAD |  |  | FROM THE WEST |  |  | WYSE ROAD |  |  | WYSE ROAD |  |  |  |
|  |  | FROM THE EAST |  |  |  |  |  | FROM THE NORTH |  |  | FROM THE SOUTH |  |  | TOTAL |
|  |  | L | S | R | L | S | R | L | S | R | L | S | R |  |
| 04:00:00 PM | 04:15:00 PM | 30 | 0 | 15 | 0 | 0 | 0 | 16 | 63 | 0 | 0 | 97 | 107 | 328 |
| 04:15:00 PM | 04:30:00 PM | 41 | 0 | 16 | 0 | 0 | 0 | 11 | 91 | 0 | 0 | 115 | 100 | 374 |
| 04:30:00 PM | 04:45:00 PM | 44 | 0 | 14 | 0 | 0 | 0 | 10 | 77 | 0 | 0 | 91 | 89 | 325 |
| 04:45:00 PM | 05:00:00 PM | 34 | 0 | 15 | 0 | 0 | 0 | 16 | 91 | 0 | 0 | 82 | 84 | 322 |
| TOTAL PEAK <br> 15 MIN PEAK <br> PEAK HOUR FACTOR TWO WAY TOTALS |  | 149 | 0 | 60 | 0 | 0 | 0 | 53 | 322 | 0 | 0 | 385 | 380 | 1349 |
|  |  | 209 |  |  | 0 |  |  | 375 |  |  | 765 |  |  |  |
|  |  | 232 |  |  | 0 |  |  | 428 |  |  | 860 |  |  |  |
|  |  | 0.9 |  |  | 0 |  |  | 0.88 |  |  | 0.89 |  |  |  |
|  |  | 642 |  |  | 0 |  |  | 820 |  |  | 1236 |  |  | FACTOR |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1 |
| DAY |  | MONTH YEAR |  |  |  |  |  |  |  |  |  |  |  | 1349 |
| WED | 7 | SEPT | 2016 |  |  |  |  |  |  |  |  |  |  |  |
| TIME: <br> 15 MIN INTERVALS |  | FROM THE EAST |  |  | FROM THE WEST |  |  | FROM THE NORTH |  |  | FROM THE SOUTH |  |  | TOTAL |
|  |  | L | S | R | L | S | R | L | S | R | L | S | R |  |
| 05:00:00 PM | 05:15:00 PM | 48 | 0 | 20 | 0 | 0 | 0 | 21 | 111 | 0 | 0 | 99 | 85 | 384 |
| 05:15:00 PM | 05:30:00 PM | 45 | 0 | 18 | 0 | 0 | 0 | 14 | 90 | 0 | 0 | 99 | 78 | 344 |
| 05:30:00 PM | 05:45:00 PM | 56 | 0 | 15 | 0 | 0 | 0 | 21 | 76 | 0 | 0 | 91 | 61 | 320 |
| 05:45:00 PM | 06:00:00 PM | 39 | 0 | 15 | 0 | 0 | 0 | 8 | 68 | 0 | 0 | 97 | 67 | 294 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| TOTAL |  | 188 | 0 | 68 | 0 | 0 | 0 | 64 | 345 | 0 | 0 | 386 | 291 | 1342 |
| PEAK |  | 256 |  |  | 0 |  |  | 409 |  |  | 677 |  |  |  |
| 15 MIN PEAK |  | 284 |  |  | 0 |  |  | 528 |  |  | 736 |  |  |  |
| PEAK HOUR | FACTOR | 0.9 |  |  | 0 |  |  | 0.77 |  |  | 0.92 |  |  |  |
| TWO WAY TOTALS |  | 611 |  |  | 0 |  |  | 863 |  |  | 1210 |  |  | FACTOR |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1 |
|  |  | 1342 |  |  |  |  |



Turning Movement Data

| Start Time | Wyse Road Southbound Southbound |  |  |  |  |  | Nantucket Ave Westbound Westbound |  |  |  |  |  | Wyse Road Northbound Northbound |  |  |  |  |  | Macdonald Bridge Eastbound Eastbound |  |  |  |  |  | Int. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Right | Thru | Left | U-Turn | Peds | $\begin{aligned} & \text { App. } \\ & \text { Total } \end{aligned}$ | Right | Thru | Left | U-Turn | Peds | App. | Right | Thru | Left | U-Turn | Peds | $\begin{aligned} & \text { App. } \\ & \text { Total } \end{aligned}$ | Right | Thru | Left | U-Turn | Peds | $\begin{aligned} & \text { App. } \\ & \text { Total } \end{aligned}$ |  |
| 7:00 AM | 175 | 15 | 7 | 0 | 0 | 197 | 2 | 212 | 0 | 0 | 3 | 214 | 2 | 13 | 196 | 0 | 1 | 211 | 100 | 52 | 34 | 0 | 3 | 186 | 808 |
| 7:15 AM | 201 | 21 | 18 | 0 | 2 | 240 | 3 | 196 | 0 | 0 | 2 | 199 | 6 | 19 | 197 | 0 | 5 | 222 | 120 | 66 | 45 | 0 | 7 | 231 | 892 |
| 7:30 AM | 140 | 16 | 19 | 0 | 0 | 175 | 2 | 243 | 0 | 0 | 2 | 245 | 6 | 23 | 212 | 0 | 1 | 241 | 120 | 56 | 36 | 0 | 6 | 212 | 873 |
| 7:45 AM | 177 | 28 | 15 | 0 | 0 | 220 | 2 | 225 | 0 | 0 | 0 | 227 | 6 | 16 | 221 | 0 | 2 | 243 | 125 | 53 | 25 | 0 | 6 | 203 | 893 |
| Hourly Total | 693 | 80 | 59 | 0 | 2 | 832 | 9 | 876 | 0 | 0 | 7 | 885 | 20 | 71 | 826 | 0 | 9 | 917 | 465 | 227 | 140 | 0 | 22 | 832 | 3466 |
| 8:00 AM | 147 | 20 | 14 | 0 | 1 | 181 | 1 | 239 | 0 | 0 | 6 | 240 | 10 | 25 | 173 | 0 | 0 | 208 | 118 | 79 | 37 | 0 | 6 | 234 | 863 |
| 8:15 AM | 143 | 34 | 12 | 0 | 1 | 189 | 10 | 194 | 0 | 0 | 6 | 204 | 10 | 27 | 176 | 0 | 4 | 213 | 142 | 61 | 31 | 0 | 5 | 234 | 840 |
| 8:30 AM | 130 | 40 | 19 | 0 | 1 | 189 | 7 | 192 | 0 | 0 | 2 | 199 | 9 | 24 | 161 | 0 | 4 | 194 | 138 | 82 | 41 | 0 | 5 | 261 | 843 |
| 8:45 AM | 127 | 40 | 21 | 0 | 2 | 188 | 5 | 155 | 1 | 0 | 2 | 161 | 10 | 32 | 124 | 0 | 1 | 166 | 131 | 56 | 43 | 0 | 2 | 230 | 745 |
| Hourly Total | 547 | 134 | 66 | 0 | 5 | 747 | 23 | 780 | 1 | 0 | 16 | 804 | 39 | 108 | 634 | 0 | 9 | 781 | 529 | 278 | 152 | 0 | 18 | 959 | 3291 |
| *** BREAK *** | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 11:00 AM | 80 | 40 | 11 | 0 | 0 | 131 | 8 | 74 | 0 | 0 | 7 | 82 | 15 | 21 | 72 | 0 | 6 | 108 | 119 | 93 | 48 | 0 | 0 | 260 | 581 |
| 11:15 AM | 74 | 23 | 17 | 0 | 0 | 114 | 19 | 78 | 0 | 0 | 5 | 97 | 10 | 21 | 88 | 0 | 4 | 119 | 100 | 94 | 50 | 0 | 1 | 244 | 574 |
| 11:30 AM | 76 | 32 | 13 | 0 | 0 | 121 | 10 | 83 | 0 | 0 | 5 | 93 | 15 | 26 | 118 | 0 | 3 | 159 | 128 | 98 | 61 | 0 | 1 | 287 | 660 |
| 11:45 AM | 70 | 33 | 17 | 0 | 0 | 120 | 21 | 88 | 0 | 0 | 2 | 109 | 19 | 42 | 87 | 0 | 1 | 148 | 96 | 99 | 72 | 0 | 5 | 267 | 644 |
| Hourly Total | 300 | 128 | 58 | 0 | 0 | 486 | 58 | 323 | 0 | 0 | 19 | 381 | 59 | 110 | 365 | 0 | 14 | 534 | 443 | 384 | 231 | 0 | 7 | 1058 | 2459 |
| 12:00 PM | 68 | 40 | 14 | 0 | 0 | 122 | 12 | 99 | 1 | 0 | 9 | 112 | 15 | 35 | 92 | 0 | 2 | 142 | 109 | 93 | 79 | 0 | 3 | 281 | 657 |
| 12:15 PM | 86 | 30 | 14 | 0 | 0 | 130 | 12 | 72 | 0 | 0 | 3 | 84 | 6 | 50 | 113 | 0 | 4 | 169 | 100 | 114 | 69 | 0 | 5 | 283 | 666 |
| 12:30 PM | 74 | 55 | 19 | 0 | 0 | 148 | 23 | 85 | 0 | 0 | 13 | 108 | 10 | 34 | 93 | 0 | 4 | 137 | 119 | 80 | 51 | 0 | 2 | 250 | 643 |
| 12:45 PM | 79 | 42 | 17 | 0 | 0 | 138 | 15 | 97 | 0 | 0 | 2 | 112 | 13 | 48 | 93 | 0 | 5 | 154 | 147 | 91 | 66 | 0 | 7 | 304 | 708 |
| Hourly Total | 307 | 167 | 64 | 0 | 0 | 538 | 62 | 353 | 1 | 0 | 27 | 416 | 44 | 167 | 391 | 0 | 15 | 602 | 475 | 378 | 265 | 0 | 17 | 1118 | 2674 |
| *** BREAK *** | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 4:00 PM | 90 | 39 | 17 | 0 | 0 | 146 | 3 | 122 | 0 | 0 | 2 | 125 | 11 | 37 | 106 | 0 | 5 | 154 | 205 | 164 | 82 | 0 | 2 | 451 | 876 |
| 4:15 PM | 71 | 33 | 10 | 0 | 1 | 114 | 8 | 153 | 0 | 0 | 3 | 161 | 6 | 37 | 128 | 0 | 4 | 171 | 233 | 148 | 63 | 0 | 12 | 444 | 890 |
| 4:30 PM | 87 | 46 | 16 | 0 | 0 | 149 | 3 | 145 | 1 | 0 | 5 | 149 | 11 | 47 | 106 | 0 | 6 | 164 | 231 | 116 | 71 | 0 | 9 | 418 | 880 |
| 4:45 PM | 93 | 38 | 12 | 0 | 2 | 143 | 9 | 145 | 0 | 0 | 6 | 154 | 4 | 41 | 95 | 0 | 6 | 140 | 238 | 181 | 72 | 0 | 3 | 491 | 928 |
| Hourly Total | 341 | 156 | 55 | 0 | 3 | 552 | 23 | 565 | 1 | 0 | 16 | 589 | 32 | 162 | 435 | 0 | 21 | 629 | 907 | 609 | 288 | 0 | 26 | 1804 | 3574 |
| 5:00 PM | 100 | 31 | 15 | 0 | 0 | 146 | 6 | 128 | 0 | 0 | 1 | 134 | 7 | 50 | 115 | 0 | 1 | 172 | 244 | 147 | 64 | 0 | 1 | 455 | 907 |
| 5:15 PM | 88 | 27 | 22 | 0 | 0 | 137 | 5 | 143 | 0 | 0 | 3 | 148 | 5 | 32 | 122 | 0 | 5 | 159 | 253 | 173 | 77 | 0 | 0 | 503 | 947 |
| 5:30 PM | 94 | 32 | 7 | 0 | 0 | 133 | 2 | 127 | 0 | 0 | 1 | 129 | 10 | 19 | 115 | 0 | 0 | 144 | 276 | 153 | 70 | 0 | 0 | 499 | 905 |
| 5:45 PM | 69 | 31 | 22 | 0 | 0 | 122 | 5 | 146 | 0 | 0 | 3 | 151 | 5 | 25 | 126 | 0 | 3 | 156 | 206 | 146 | 74 | 0 | 0 | 426 | 855 |
| Hourly Total | 351 | 121 | 66 | 0 | 0 | 538 | 18 | 544 | 0 | 0 | 8 | 562 | 27 | 126 | 478 | 0 | 9 | 631 | 979 | 619 | 285 | 0 | 1 | 1883 | 3614 |
| Grand Total | 2539 | 786 | 368 | 0 | 10 | 3693 | 193 | 3441 | 3 | 0 | 93 | 3637 | 221 | 744 | 3129 | 0 | 77 | 4094 | 3798 | 2495 | 1361 | 0 | 91 | 7654 | 19078 |
| Approach \% | 68.8 | 21.3 | 10.0 | 0.0 | - | - | 5.3 | 94.6 | 0.1 | 0.0 | - | - | 5.4 | 18.2 | 76.4 | 0.0 | - | - | 49.6 | 32.6 | 17.8 | 0.0 | - | - | - |
| Total \% | 13.3 | 4.1 | 1.9 | 0.0 | - | 19.4 | 1.0 | 18.0 | 0.0 | 0.0 | - | 19.1 | 1.2 | 3.9 | 16.4 | 0.0 | - | 21.5 | 19.9 | 13.1 | 7.1 | 0.0 | - | 40.1 | - |
| All Vehicles (no classification) | 2539 | 786 | 368 | 0 | - | 3693 | 193 | 3441 | 3 | 0 | - | 3637 | 221 | 744 | 3129 | 0 | - | 4094 | 3798 | 2495 | 1361 | 0 | - | 7654 | 19078 |
| \% All Vehicles (no classification) | 100.0 | 100.0 | 100.0 | - | - | 100.0 | 100.0 | 100.0 | 100.0 | - | - | 100.0 | 100.0 | 100.0 | 100.0 | - | - | 100.0 | 100.0 | 100.0 | 100.0 | - | - | 100.0 | 100.0 |
| Bicycles on Crosswalk | - | - | - | - | 3 | - | - | - | - | - | 2 | - | - | - | - | - | 0 | - | - | - | - | - | 5 | - | - |

## Turning Movement Peak Hour Data (7:15 AM)

| Start Time | Wyse Road Southbound Southbound |  |  |  |  |  | Nantucket Ave Westbound Westbound |  |  |  |  |  | Wyse Road Northbound Northbound |  |  |  |  |  | Macdonald Bridge Eastbound Eastbound |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Right | Thru | Left | U-Turn | Peds | App. Total | Right | Thru | Left | U-Turn | Peds | App. Total | Right | Thru | Left | U-Turn | Peds | App. Total | Right | Thru | Left | U-Turn | Peds | App. Total | Int. Total |
| 7:15 AM | 201 | 21 | 18 | 0 | 2 | 240 | 3 | 196 | 0 | 0 | 2 | 199 | 6 | 19 | 197 | 0 | 5 | 222 | 120 | 66 | 45 | 0 | 7 | 231 | 892 |
| 7:30 AM | 140 | 16 | 19 | 0 | 0 | 175 | 2 | 243 | 0 | 0 | 2 | 245 | 6 | 23 | 212 | 0 | 1 | 241 | 120 | 56 | 36 | 0 | 6 | 212 | 873 |
| 7:45 AM | 177 | 28 | 15 | 0 | 0 | 220 | 2 | 225 | 0 | 0 | 0 | 227 | 6 | 16 | 221 | 0 | 2 | 243 | 125 | 53 | 25 | 0 | 6 | 203 | 893 |
| 8:00 AM | 147 | 20 | 14 | 0 | 1 | 181 | 1 | 239 | 0 | 0 | 6 | 240 | 10 | 25 | 173 | 0 | 0 | 208 | 118 | 79 | 37 | 0 | 6 | 234 | 863 |
| Total | 665 | 85 | 66 | 0 | 3 | 816 | 8 | 903 | 0 | 0 | 10 | 911 | 28 | 83 | 803 | 0 | 8 | 914 | 483 | 254 | 143 | 0 | 25 | 880 | 3521 |
| Approach \% | 81.5 | 10.4 | 8.1 | 0.0 | - | - | 0.9 | 99.1 | 0.0 | 0.0 | - | - | 3.1 | 9.1 | 87.9 | 0.0 | - | - | 54.9 | 28.9 | 16.3 | 0.0 | - | - | - |
| Total \% | 18.9 | 2.4 | 1.9 | 0.0 | - | 23.2 | 0.2 | 25.6 | 0.0 | 0.0 | - | 25.9 | 0.8 | 2.4 | 22.8 | 0.0 | - | 26.0 | 13.7 | 7.2 | 4.1 | 0.0 | - | 25.0 | - |
| PHF | 0.827 | 0.759 | 0.868 | 0.000 | - | 0.850 | 0.667 | 0.929 | 0.000 | 0.000 | - | 0.930 | 0.700 | 0.830 | 0.908 | 0.000 | - | 0.940 | 0.966 | 0.804 | 0.794 | 0.000 | - | 0.940 | 0.986 |
| All Vehicles (no classification) | 665 | 85 | 66 | 0 | - | 816 | 8 | 903 | 0 | 0 | - | 911 | 28 | 83 | 803 | 0 | - | 914 | 483 | 254 | 143 | 0 | - | 880 | 3521 |
| \% All Vehicles (no classification) | 100.0 | 100.0 | 100.0 | - | - | 100.0 | 100.0 | 100.0 | - | - | - | 100.0 | 100.0 | 100.0 | 100.0 | - | - | 100.0 | 100.0 | 100.0 | 100.0 | - | - | 100.0 | 100.0 |
| Bicycles on Crosswalk | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - | - | - | - | 2 | - | - |
| \% Bicycles on Crosswalk | - | - | - | - | 0.0 | - | - | - | - | - | 0.0 | - | - | - | - | - | 0.0 | - | - | - | - | - | 8.0 | - | - |
| Pedestrians | - | - | - | - | 3 | - | - | - | - | - | 10 | - | - | - | - | - | 8 | - | - | - | - | - | 23 | - | - |
| \% Pedestrians | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 92.0 | - | - |



Turning Movement Peak Hour Data Plot (7:15 AM)

## Turning Movement Peak Hour Data (4:45 PM)

| Start Time | Wyse Road Southbound Southbound |  |  |  |  |  | Nantucket Ave Westbound Westbound |  |  |  |  |  | Wyse Road Northbound Northbound |  |  |  |  |  | Macdonald Bridge Eastbound Eastbound |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Right | Thru | Left | U-Turn | Peds | App. Total | Right | Thru | Left | U-Turn | Peds | App. Total | Right | Thru | Left | U-Turn | Peds | App. Total | Right | Thru | Left | U-Turn | Peds | $\begin{aligned} & \text { App. } \\ & \text { Total } \end{aligned}$ | Int. Total |
| 4:45 PM | 93 | 38 | 12 | 0 | 2 | 143 | 9 | 145 | 0 | 0 | 6 | 154 | 4 | 41 | 95 | 0 | 6 | 140 | 238 | 181 | 72 | 0 | 3 | 491 | 928 |
| 5:00 PM | 100 | 31 | 15 | 0 | 0 | 146 | 6 | 128 | 0 | 0 | 1 | 134 | 7 | 50 | 115 | 0 | 1 | 172 | 244 | 147 | 64 | 0 | 1 | 455 | 907 |
| 5:15 PM | 88 | 27 | 22 | 0 | 0 | 137 | 5 | 143 | 0 | 0 | 3 | 148 | 5 | 32 | 122 | 0 | 5 | 159 | 253 | 173 | 77 | 0 | 0 | 503 | 947 |
| 5:30 PM | 94 | 32 | 7 | 0 | 0 | 133 | 2 | 127 | 0 | 0 | 1 | 129 | 10 | 19 | 115 | 0 | 0 | 144 | 276 | 153 | 70 | 0 | 0 | 499 | 905 |
| Total | 375 | 128 | 56 | 0 | 2 | 559 | 22 | 543 | 0 | 0 | 11 | 565 | 26 | 142 | 447 | 0 | 12 | 615 | 1011 | 654 | 283 | 0 | 4 | 1948 | 3687 |
| Approach \% | 67.1 | 22.9 | 10.0 | 0.0 | - | - | 3.9 | 96.1 | 0.0 | 0.0 | - | - | 4.2 | 23.1 | 72.7 | 0.0 | - | - | 51.9 | 33.6 | 14.5 | 0.0 | - | - | - |
| Total \% | 10.2 | 3.5 | 1.5 | 0.0 | - | 15.2 | 0.6 | 14.7 | 0.0 | 0.0 | - | 15.3 | 0.7 | 3.9 | 12.1 | 0.0 | - | 16.7 | 27.4 | 17.7 | 7.7 | 0.0 | - | 52.8 | - |
| PHF | 0.938 | 0.842 | 0.636 | 0.000 | - | 0.957 | 0.611 | 0.936 | 0.000 | 0.000 | - | 0.917 | 0.650 | 0.710 | 0.916 | 0.000 | - | 0.894 | 0.916 | 0.903 | 0.919 | 0.000 | - | 0.968 | 0.973 |
| All Vehicles (no classification) | 375 | 128 | 56 | 0 | - | 559 | 22 | 543 | 0 | 0 | - | 565 | 26 | 142 | 447 | 0 | - | 615 | 1011 | 654 | 283 | 0 | - | 1948 | 3687 |
| \% All Vehicles (no classification) | 100.0 | 100.0 | 100.0 | - | - | 100.0 | 100.0 | 100.0 | - | - | - | 100.0 | 100.0 | 100.0 | 100.0 | - | - | 100.0 | 100.0 | 100.0 | 100.0 | - | - | 100.0 | 100.0 |
| Bicycles on Crosswalk | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - |
| \% Bicycles on Crosswalk | - | - | - | - | 0.0 | - | - | - | - | - | 0.0 | - | - | - | - | - | 0.0 | - | - | - | - | - | 0.0 | - | - |
| Pedestrians | - | - | - | - | 2 | - | - | - | - | - | 11 | - | - | - | - | - | 12 | - | - | - | - | - | 4 | - | - |
| \% Pedestrians | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - |



Turning Movement Peak Hour Data Plot (4:45 PM)

## MANUAL TRAFFIC COUNTS




## MANUAL TRAFFIC COUNTS

| INTERSECTION DAY | N: | THISTLE STREET AT WYSE ROAD |  |  |  |  |  |  | WEATHER RECORDER |  |  | $\begin{gathered} \hline \text { SUNNY } \\ \hline \text { KS } \end{gathered}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MONTH YEAR |  |  |  |  |  |  |  |  |  |  |  |  |
| THURS | 24 | AUG | 2017 |  |  |  |  |  |  |  |  |  |  |  |
| STREET: <br> TIME: <br> 15 MIN INT | RVALS | THISTLE STREET |  |  |  |  |  | WYSE ROAD |  |  | WYSE ROAD |  |  |  |
|  |  | FROM THE EAST |  |  | FROM THE WEST |  |  | FROM THE NORTH |  |  | FROM THE SOUTH |  |  | TOTAL |
|  |  | L | S | R | L | S | R | L | S | R | L | S | R |  |
| 04:00:00 PM | 04:15:00 PM | 3 | 0 | 71 | 0 | 0 | 0 | 25 | 153 | 0 | 0 | 122 | 6 | 380 |
| 04:15:00 PM | 04:30:00 PM | 14 | 0 | 53 | 0 | 0 | 0 | 51 | 179 | 0 | 0 | 153 | 5 | 455 |
| 04:30:00 PM | 04:45:00 PM | 17 | 0 | 49 | 0 | 0 | 0 | 86 | 184 | 0 | 0 | 150 | 9 | 495 |
| 04:45:00 PM | 05:00:00 PM | 20 | 0 | 50 | 0 | 0 | 0 | 89 | 165 | 0 | 0 | 159 | 10 | 493 |
| TOTAL |  | 54 | 0 | 223 | 0 | 0 | 0 | 251 | 681 | 0 | 0 | 584 | 30 | 1823 |
| PEAK |  | 277 |  |  | 0 |  |  | 932 |  |  | 614 |  |  |  |
| 15 MIN PEAK |  | 296 |  |  | 0 |  |  | 1080 |  |  | 676 |  |  |  |
| PEAK HOUR | FACTOR | 0.94 |  |  | 0 |  |  | 0.86 |  |  | 0.91 |  |  |  |
| TWO WAY TOTALS |  | 558 |  |  | 0 |  |  | 1739 |  |  | 1349 |  |  | FACTOR |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1.02 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1859 |
| DAY | DATE | MONTH YEAR |  |  |  |  |  |  |  |  |  |  |  |  |
| THURS | 24 | AUG 2017 |  |  |  |  |  |  |  |  |  |  |  |  |
| TIME:15 MIN INTERVALS |  | FROM THE EAST |  |  | FROM THE WEST |  |  | FROM THE NORTH |  |  | FROM THE SOUTH |  |  | TOTAL |
|  |  | L | S | R | L | S | R | L | S | R | L | S | R |  |
| 05:00:00 PM | 05:15:00 PM | 19 | 0 | 45 | 0 | 0 | 0 | 92 | 162 | 0 | 0 | 162 | 14 | 494 |
| 05:15:00 PM | 05:30:00 PM | 15 | 0 | 43 | 0 | 0 | 0 | 89 | 171 | 0 | 0 | 167 | 15 | 500 |
| 05:30:00 PM | 05:45:00 PM | $16$ | 0 | 40 | 0 | 0 | 0 | 88 | 180 | 0 | 0 | 171 | 17 | 512 |
| 05:45:00 PM | 06:00:00 PM | 19 | 0 | 41 | 0 | 0 | 0 | 86 | 161 | 0 | 0 | 158 | 15 | 480 |
| TOTAL |  | $69$ |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | 0 | 169 | 0 | 0 | 0 | 355 | 674 | 0 | 0 | 658 | 61 | 1986 |  |
| PEAK <br> 15 MIN PEAK |  |  |  |  |  | 0 |  |  | 1029 |  |  | 719 |  |  |  |
|  |  | 238256 |  |  | 0 |  |  | 1072 |  |  | 752 |  |  |  |
| PEAK HOUR FACTOR |  | 0.93 |  |  | 0 |  |  | 0.96 |  |  | 0.96 |  |  |  |
| TWO WAY TOTALS |  | 654 |  |  | 0 |  |  | 1856 |  |  | 1462 |  |  | FACTOR |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1.02 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2026 |



## MANUAL TRAFFIC COUNTS




## MANUAL TRAFFIC COUNTS

| INTERSECTION: |  | WINDMILL ROAD AT WYSE ROAD |  |  |  |  |  |  | WEATHER RECORDER |  |  | SUNNY |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DAY | DATE | MONTH | YEAR |  |  |  |  |  |  |  |  |  |  |  |
| THURS | 2 | NOV | 2017 |  |  |  |  |  |  |  |  |  |  |  |
| STREET: <br> TIME: <br> 15 MIN INTERVALS |  | WYSE ROAD |  |  | FROM THE WEST |  |  | WINDMILL ROAD |  |  | WINDMILL ROAD |  |  |  |
|  |  | FROM THE EAST |  |  |  |  |  | FROM THE NORTH |  |  | FROM THE SOUTH |  |  | TOTAL |
|  |  | L | S | R | L | S | R | L | S | R | L | S | R |  |
| 04:00:00 PM | 04:15:00 PM | 97 | 0 | 11 | 0 | 0 | 0 | 3 | 45 | 0 | 0 | 30 | 131 | 317 |
| 04:15:00 PM | 04:30:00 PM | 123 | 0 | 8 | 0 | 0 | 0 | 7 | 51 | 0 | 0 | 52 | 140 | 381 |
| 04:30:00 PM | 04:45:00 PM | 99 | 0 | 5 | 0 | 0 | 0 | 2 | 56 | 0 | 0 | 69 | 143 | 374 |
| 04:45:00 PM | 05:00:00 PM | 102 | 0 | 7 | 0 | 0 | 0 | 5 | 43 | 0 | 0 | 72 | 138 | 367 |
| TOTAL |  | 421 | 0 | 31 | 0 | 0 | 0 | 17 | 195 | 0 | 0 | 223 | 552 | 1439 |
| PEAK |  | 452 |  |  | 0 |  |  | 212 |  |  | 775 |  |  |  |
| 15 MIN PEAK |  | 524 |  |  | 0 |  |  | 232 |  |  | 848 |  |  |  |
| PEAK HOUR | FACTOR | 0.86 |  |  | 0 |  |  | 0.91 |  |  | 0.91 |  |  |  |
| TWO WAY TOTALS |  | 1021 |  |  | 0 |  |  | 466 |  |  | 1391 |  |  | FACTOR |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0.97 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1396 |
| DAY | DATE | MONTH YEAR |  |  |  |  |  |  |  |  |  |  |  |  |
| THURS | 2 | NOV | 2017 |  |  |  |  |  |  |  |  |  |  |  |



TOTAL
PEAK
15 MIN PEAK
PEAK HOUR FACTOR
TWO WAY TOTALS

| 477 | 0 | 35 | 0 | 0 | 0 | 37 | 239 | 0 | 0 | 299 | 557 | 1644 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 512 |  |  | 0 |  |  | 276 |  |  | 856 |  |  |
|  | 572 |  |  | 0 |  |  | 304 |  |  | 944 |  |  |
|  | 0.9 |  |  | 0 |  |  | 0.91 |  |  | 0.91 |  |  |
|  | 1106 |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  | 1572 |  |  |  |  |  |  |
| FACTOR |  |  |  |  |  |  |  |  |  |  |  |  |




## APPENDIX B

## Trip Generation

Trip Generation Summary

Alternative: Alternative 1

| Phase: | Open Date: | 2019-11-10 |
| :--- | ---: | ---: |
| Project: | Wyse Road Development | Analysis Date: |


|  | Land Use |  | * | Enter | Exit | Total | * | Enter | Exit | Total | * | Enter | Exit | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Multifamily (High Rise) |  |  | 352 | 352 | 704 |  | 12 | 36 | 48 |  | 31 | 20 | 51 |
|  | 125 | Dwelling Units |  |  |  |  |  |  |  |  |  |  |  |  |
| 710 | Office |  |  | 39 | 39 | 78 |  | 8 | 1 | 9 |  | 1 | 8 | 9 |
|  | 8 | 1000 Sq. Ft. GFA |  |  |  |  |  |  |  |  |  |  |  |  |
| 820 | Retail |  |  | 170 | 170 | 340 |  | 5 | 3 | 8 |  | 16 | 18 | 34 |
|  | 9 | 1000 Sq. Ft. GLA |  |  |  |  |  |  |  |  |  |  |  |  |
| Unadjusted Volume |  |  |  | 561 | 561 | 1122 |  | 25 | 40 | 65 |  | 48 | 46 | 94 |
| Internal Capture Trips |  |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 9 | 9 | 18 |
| Pass-By Trips |  |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 4 | 4 | 8 |
| Volume Added to Adjacent Streets |  |  |  | 561 | 561 | 1122 |  | 25 | 40 | 65 |  | 35 | 33 | 68 |

Total Weekday Average Daily Trips Internal Capture $=0$ Percent
Total Weekday AM Peak Hour of Adjacent Street Traffic Internal Capture $=0$ Percent
Total Weekday PM Peak Hour of Adjacent Street Traffic Internal Capture $=19$ Percent


## APPENDIX C

## Trip Assignment

## Development: Wyse Road Development

Driveway: 1 Development - Nantucket

| Origin \# | Route | To |  | From |  |
| :---: | :--- | :---: | :---: | :---: | :---: |
|  |  | Distribution \% | Trips | Distribution \% | Trips |
| 1 | NW Victoria to Development - Nantucket | 20.00 | 5 | 20.00 | 8 |
| 2 | N School to Development - Nantucket | 5.00 | 1 | 5.00 | 2 |
| 3 | NE Thistle to Development - Nantucket | 5.00 | 1 | 5.00 | 2 |
| 4 | NE Victoria to Development - Nantucket | 5.00 | 1 | 5.00 | 2 |
| 5 | SE Alderney to Development - Nantucket | 10.00 | 3 | 10.00 | 4 |
| 6 | SE Windmill to Development - Nantucket | 5.00 | 1 | 5.00 | 2 |
| 7 | S Macdonald Bridge to Development - Nantucket | 40.00 | 10 | 40.00 | 16 |
| 8 | W Wyse to Development - Nantucket | 10.00 | 3 | 10.00 | 4 |

## Development: Wyse Road Development

Driveway: 1 Development - Nantucket

| Origin \# | Route | To |  | From |  |
| :---: | :--- | :---: | :---: | :---: | :---: |
|  |  | Distribution \% | Trips | Distribution \% | Trips |
| 1 | NW Victoria to Development - Nantucket | 20.00 | 8 | 37.34 | 14 |
| 2 | N School to Development - Nantucket | 5.00 | 2 | 3.25 | 1 |
| 3 | NE Thistle to Development - Nantucket | 5.00 | 2 | 0.00 | 0 |
| 4 | NE Victoria to Development - Nantucket | 5.00 | 2 | 0.00 | 0 |
| 5 | SE Alderney to Development - Nantucket | 10.00 | 4 | 15.33 | 6 |
| 6 | SE Windmill to Development - Nantucket | 5.00 | 2 | 3.99 | 1 |
| 7 | S Macdonald Bridge to Development - Nantucket | 40.00 | 16 | 40.09 | 15 |
| 8 | SW Wyse to Development - Nantucket | 10.00 | 4 | 0.00 | 0 |



## APPENDIX D

## Synchro Output



|  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBR | WBT | NBL | NBT | NBR | SBL | SBT |
| Lane Configurations | 7 | \& |  | ¢ ${ }^{\text {¢ }}$ | F |  | * ${ }^{\text {d }}$ |
| Traffic Volume (vph) | 5 | 4 | 24 | 280 | 44 | 20 | 939 |
| Future Volume (vph) | 5 | 4 | 24 | 280 | 44 | 20 | 939 |
| Lane Group Flow (vph) | 5 | 49 | 0 | 330 | 48 | 0 | 1107 |
| Turn Type | Perm | NA | Perm | NA | Perm | Perm | NA |
| Protected Phases |  | 8 |  | 2 |  |  | 6 |
| Permitted Phases | 4 |  | 2 |  | 2 | 6 |  |
| Minimum Split (s) | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 |
| Total Split (s) | 25.0 | 25.0 | 65.0 | 65.0 | 65.0 | 65.0 | 65.0 |
| Total Split (\%) | 27.8\% | 27.8\% | 72.2\% | 72.2\% | 72.2\% | 72.2\% | 72.2\% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 |
| Total Lost Time (s) | 4.5 | 4.5 |  | 4.5 | 4.5 |  | 4.5 |
| Lead/Lag |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |
| Act Effct Green (s) | 20.5 | 20.5 |  | 60.5 | 60.5 |  | 60.5 |
| Actuated g/C Ratio | 0.23 | 0.23 |  | 0.67 | 0.67 |  | 0.67 |
| v/c Ratio | 0.01 | 0.12 |  | 0.16 | 0.04 |  | 0.50 |
| Control Delay | 0.0 | 14.2 |  | 5.7 | 1.7 |  | 8.1 |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 |
| Total Delay | 0.0 | 14.2 |  | 5.7 | 1.7 |  | 8.1 |
| LOS | A | B |  | A | A |  | A |
| Approach Delay |  | 14.2 |  | 5.2 |  |  | 8.1 |
| Approach LOS |  | B |  | A |  |  | A |
| Queue Length 50th (m) | 0.0 | 1.7 |  | 10.2 | 0.0 |  | 45.0 |
| Queue Length 95th (m) | 0.0 | m8.3 |  | 15.2 | 3.3 |  | 58.6 |
| Internal Link Dist (m) |  | 136.0 |  | 20.6 |  |  | 158.1 |
| Turn Bay Length (m) |  |  |  |  |  |  |  |
| Base Capacity (vph) | 481 | 406 |  | 2007 | 1079 |  | 2230 |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 |
| Reduced v/c Ratio | 0.01 | 0.12 |  | 0.16 | 0.04 |  | 0.50 |
| Intersection Summary |  |  |  |  |  |  |  |
| Cycle Length: 90 |  |  |  |  |  |  |  |
| Actuated Cycle Length: 90 |  |  |  |  |  |  |  |
| Offset: 0 (0\%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green |  |  |  |  |  |  |  |
| Natural Cycle: 50 |  |  |  |  |  |  |  |
| Control Type: Pretimed |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.50 |  |  |  |  |  |  |  |
| Intersection Signal Delay: 7.5 |  |  |  | Intersection LOS: A |  |  |  |
| Intersection Capacity Utilization 52.3\% |  |  |  | ICU Level of Service A |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |

$m$ Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 3: Nantucket \& Mall/Sportsplex




|  | 4 | $\rightarrow$ | $\cdots$ | 7 |  | $4$ | $4$ | 4 | $p$ |  | $\frac{1}{7}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | 「 |  |  | T |  | 44 | T |  | 中t |  |
| Trafic Volume (veh/h) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 348 | , | 0 | 911 | 36 |
| Future Volume (Veh/h) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 348 | 0 | 0 | 911 | 36 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | -5\% |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 378 | 0 | 0 | 990 | 39 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (m) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (m/s) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | None |  |  | None |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal (m) |  |  |  |  |  |  |  | 53 |  |  | 45 |  |
| pX, platoon unblocked | 0.87 | 0.87 | 0.85 | 0.87 | 0.87 | 0.96 | 0.85 |  |  | 0.96 |  |  |
| vC , conflicting volume | 1198 | 1388 | 514 | 873 | 1407 | 189 | 1029 |  |  | 378 |  |  |
| VC 1 , stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu , unblocked vol | 739 | 957 | 78 | 365 | 979 | 84 | 683 |  |  | 280 |  |  |
| tC, single (s) | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 |  |  | 4.1 |  |  |
| $\mathrm{tC}, 2$ stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \% | 100 | 100 | 100 | 100 | 100 | 100 | 100 |  |  | 100 |  |  |
| cM capacity (veh/h) | 265 | 223 | 822 | 492 | 216 | 924 | 771 |  |  | 1234 |  |  |
| Direction, Lane \# | EB 1 | WB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 |  |  |  |  |  |
| Volume Total | 0 | 0 | 189 | 189 | 0 | 660 | 369 |  |  |  |  |  |
| Volume Left | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |  |  |
| Volume Right | 0 | 0 | 0 | 0 | 0 | 0 | 39 |  |  |  |  |  |
| cSH | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |  |  |  |  |  |
| Volume to Capacity | 0.04 | 0.05 | 0.11 | 0.11 | 0.02 | 0.39 | 0.22 |  |  |  |  |  |
| Queue Length 95th (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |  |  |
| Control Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |  |  |
| Lane LOS | A | A |  |  |  |  |  |  |  |  |  |  |
| Approach Delay (s) | 0.0 | 0.0 | 0.0 |  |  | 0.0 |  |  |  |  |  |  |
| Approach LOS | A | A |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.0 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 29.7\% |  | CU Level of | Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |


|  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |





|  | $\rangle$ |  | 7 | $\checkmark$ |  |  | 4 | $\dagger$ | $p$ |  | $\frac{1}{\dagger}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | 「 |  |  | 「 |  | 44 | 「 |  | 4t |  |
| Traffic Volume（veh／h） | 0 | 0 | 0 | 0 | 0 |  | 0 | 348 | 0 | 0 | 911 | 36 |
| Future Volume（Veh／h） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 357 | 0 | 0 | 934 | 37 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | －5\％ |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate（vph） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 388 | 0 | 0 | 1015 | 40 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width（m） |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed（m／s） |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | None |  |  | None |  |
| Median storage veh） |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal（m） |  |  |  |  |  |  |  | 53 |  |  | 45 |  |
| pX，platoon unblocked | 0.86 | 0.86 | 0.84 | 0.86 | 0.86 | 0.96 | 0.84 |  |  | 0.96 |  |  |
| vC ，conflicting volume | 1229 | 1423 | 528 | 896 | 1443 | 194 | 1055 |  |  | 388 |  |  |
| vC 1 ，stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 755 | 980 | 73 | 369 | 1003 | 86 | 698 |  |  | 287 |  |  |
| tC，single（s） | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 |  |  | 4.1 |  |  |
| $\mathrm{tC}, 2$ stage（s） |  |  |  |  |  |  |  |  |  |  |  |  |
| tF（s） | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \％ | 100 | 100 | 100 | 100 | 100 | 100 | 100 |  |  | 100 |  |  |
| cM capacity（veh／h） | 257 | 215 | 822 | 486 | 208 | 921 | 756 |  |  | 1225 |  |  |
| Direction，Lane \＃ | EB 1 | WB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 |  |  |  |  |  |
| Volume Total | 0 | 0 | 194 | 194 | 0 | 677 | 378 |  |  |  |  |  |
| Volume Left | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |  |  |
| Volume Right | 0 | 0 | 0 | 0 | 0 | 0 | 40 |  |  |  |  |  |
| CSH | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |  |  |  |  |  |
| Volume to Capacity | 0.00 | 0.00 | 0.11 | 0.11 | 0.00 | 0.40 | 0.22 |  |  |  |  |  |
| Queue Length 95th（m） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |  |  |
| Control Delay（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |  |  |
| Lane LOS | A | A |  |  |  |  |  |  |  |  |  |  |
| Approach Delay（s） | 0.0 | 0.0 | 0.0 |  |  | 0.0 |  |  |  |  |  |  |
| Approach LOS | A | A |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.0 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 29．7\％ |  | Level | rvice |  |  | A |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |


$m$ Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 1: Nantucket/Maple \& Victoria


|  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBR | WBT | NBL | NBT | NBR | SBL | SBT |
| Lane Configurations | 7 | \& |  | ¢ ${ }^{\text {¢ }}$ | 7 |  | * ${ }^{\text {d }}$ |
| Traffic Volume (vph) | 5 | 4 | 24 | 280 | 44 | 20 | 939 |
| Future Volume (vph) | 5 | 4 | 25 | 326 | 47 | 21 | 963 |
| Lane Group Flow (vph) | 5 | 50 | 0 | 381 | 51 | 0 | 1135 |
| Turn Type | Perm | NA | Perm | NA | Perm | Perm | NA |
| Protected Phases |  | 8 |  | 2 |  |  | 6 |
| Permitted Phases | 4 |  | 2 |  | 2 | 6 |  |
| Minimum Split (s) | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 |
| Total Split (s) | 25.0 | 25.0 | 65.0 | 65.0 | 65.0 | 65.0 | 65.0 |
| Total Split (\%) | 27.8\% | 27.8\% | 72.2\% | 72.2\% | 72.2\% | 72.2\% | 72.2\% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 |
| Total Lost Time (s) | 4.5 | 4.5 |  | 4.5 | 4.5 |  | 4.5 |
| Lead/Lag |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |
| Act Effct Green (s) | 20.5 | 20.5 |  | 60.5 | 60.5 |  | 60.5 |
| Actuated g/C Ratio | 0.23 | 0.23 |  | 0.67 | 0.67 |  | 0.67 |
| v/c Ratio | 0.01 | 0.12 |  | 0.19 | 0.05 |  | 0.51 |
| Control Delay | 0.0 | 13.8 |  | 5.8 | 1.6 |  | 8.2 |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 |
| Total Delay | 0.0 | 13.8 |  | 5.8 | 1.6 |  | 8.2 |
| LOS | A | B |  | A | A |  | A |
| Approach Delay |  | 13.8 |  | 5.3 |  |  | 8.2 |
| Approach LOS |  | B |  | A |  |  | A |
| Queue Length 50th (m) | 0.0 | 0.8 |  | 12.0 | 0.0 |  | 46.7 |
| Queue Length 95th (m) | 0.0 | m8.3 |  | 17.5 | 3.4 |  | 60.8 |
| Internal Link Dist (m) |  | 136.0 |  | 20.6 |  |  | 158.1 |
| Turn Bay Length (m) |  |  |  |  |  |  |  |
| Base Capacity (vph) | 475 | 407 |  | 2012 | 1080 |  | 2227 |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 |
| Reduced v/c Ratio | 0.01 | 0.12 |  | 0.19 | 0.05 |  | 0.51 |
| Intersection Summary |  |  |  |  |  |  |  |
| Cycle Length: 90 |  |  |  |  |  |  |  |
| Actuated Cycle Length: 90 |  |  |  |  |  |  |  |
| Offset: 0 (0\%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green |  |  |  |  |  |  |  |
| Natural Cycle: 50 |  |  |  |  |  |  |  |
| Control Type: Pretimed |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.51 |  |  |  |  |  |  |  |
| Intersection Signal Delay: 7.6 |  |  |  | Intersection LOS: A |  |  |  |
| Intersection Capacity Utilization 52.3\% |  |  |  | ICU Level of Service A |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |

$m$ Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 3: Nantucket \& Mall/Sportsplex





|  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |




|  | $\rangle$ |  | $\leftarrow$ | ＊ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBT | SBL | SBR |
| Lane Configurations | \％ | 性 | 性 | ${ }^{7}$ | 「 |
| Traffic Volume（vph） | 362 | 687 | 671 | 70 | 172 |
| Future Volume（vph） | 362 | 687 | 671 | 70 | 172 |
| Lane Group Flow（vph） | 393 | 747 | 796 | 76 | 187 |
| Turn Type | pm＋pt | NA | NA | Prot | Perm |
| Protected Phases | 7 | 4 | 8 | 6 |  |
| Permitted Phases | 4 |  |  |  | 6 |
| Detector Phase | 7 | 4 | 8 | 6 | 6 |
| Switch Phase |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split（s） | 9.5 | 22.5 | 22.5 | 22.5 | 22.5 |
| Total Split（s） | 15.0 | 37.5 | 22.5 | 22.5 | 22.5 |
| Total Split（\％） | 25．0\％ | 62．5\％ | 37．5\％ | 37．5\％ | 37．5\％ |
| Yellow Time（s） | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All－Red Time（s） | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Lead／Lag | Lead |  | Lag |  |  |
| Lead－Lag Optimize？ | Yes |  | Yes |  |  |
| Recall Mode | None | None | None | Max | Max |
| Act Efft Green（s） | 31.8 | 31.8 | 16.8 | 18.0 | 18.0 |
| Actuated g／C Ratio | 0.54 | 0.54 | 0.29 | 0.31 | 0.31 |
| v／c Ratio | 0.89 | 0.39 | 0.79 | 0.14 | 0.30 |
| Control Delay | 37.0 | 8.6 | 25.6 | 16.2 | 4.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 37.0 | 8.6 | 25.6 | 16.2 | 4.6 |
| LOS | D | A | C | B | A |
| Approach Delay |  | 18.4 | 25.6 | 8.0 |  |
| Approach LOS |  | B | C | A |  |
| Queue Length 50th（ m ） | 26.4 | 23.3 | 42.4 | 6.4 | 0.0 |
| Queue Length 95th（ m ） | \＃73．5 | 33.6 | 61.3 | 14.9 | 12.1 |
| Internal Link Dist（ $m$ ） |  | 153.3 | 86.2 | 122.6 |  |
| Turn Bay Length（ $m$ ） |  |  |  |  | 80.0 |
| Base Capacity（vph） | 443 | 1987 | 1081 | 542 | 614 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Reduced v／c Ratio | 0.89 | 0.38 | 0.74 | 0.14 | 0.30 |
| Intersection Summary |  |  |  |  |  |
| Cycle Length： 60 |  |  |  |  |  |
| Actuated Cycle Length： 58.8 |  |  |  |  |  |
| Natural Cycle： 60 |  |  |  |  |  |
| Control Type：Actuated－Uncoordinated |  |  |  |  |  |
| Maximum v／c Ratio： 0.89 |  |  |  |  |  |
| Intersection Signal Delay： 19.8 Intection Capacity Utiization 56．0\％ |  |  |  |  | rsection LOS：B |
|  |  |  |  |  | Level of Service B |
| Analysis Period（min） 15 |  |  |  |  |  |
| \＃95th percentile volume exceeds capacity，queue may be longer．Queue shown is maximum after two cycles． |  |  |  |  |  |
|  |  |  |  |  |  |

Splits and Phases：10：Wyse \＆Thistle


|  | $\rangle$ |  | 7 | 7 |  |  | 4 | 4 | $p$ |  | $\frac{1}{\dagger}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | 「 |  |  | 「 |  | 44 | 「 |  | 4t |  |
| Traffic Volume（veh／h） | 0 | 0 | 30 | 0 | 0 |  | 0 | 764 | 0 | 0 | 448 | 20 |
| Future Volume（Veh／h） | 0 | 0 | 30 | 0 | 0 | 0 | 0 | 764 | 0 | 0 | 448 | 20 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | －5\％ |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate（vph） | 0 | 0 | 33 | 0 | 0 | 0 | 0 | 830 | 0 | 0 | 487 | 22 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width（m） |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed（m／s） |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | None |  |  | None |  |
| Median storage veh） |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal（m） |  |  |  |  |  |  |  | 53 |  |  | 45 |  |
| pX，platoon unblocked | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.91 | 0.94 |  |  | 0.91 |  |  |
| vC ，conflicting volume | 913 | 1328 | 254 | 1106 | 1339 | 415 | 509 |  |  | 830 |  |  |
| vC 1 ，stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 508 | 948 | 85 | 713 | 960 | 170 | 355 |  |  | 624 |  |  |
| tC，single（s） | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 |  |  | 4.1 |  |  |
| $\mathrm{tC}, 2$ stage（s） |  |  |  |  |  |  |  |  |  |  |  |  |
| tF（s） | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \％ | 100 | 100 | 96 | 100 | 100 | 100 | 100 |  |  | 100 |  |  |
| cM capacity（veh／h） | 422 | 244 | 901 | 289 | 240 | 771 | 1130 |  |  | 870 |  |  |
| Direction，Lane \＃ | EB 1 | WB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 |  |  |  |  |  |
| Volume Total | 33 | 0 | 415 | 415 | 0 | 325 | 184 |  |  |  |  |  |
| Volume Left | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |  |  |
| Volume Right | 33 | 0 | 0 | 0 | 0 | 0 | 22 |  |  |  |  |  |
| CSH | 901 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |  |  |  |  |  |
| Volume to Capacity | 0.04 | 0.05 | 0.24 | 0.24 | 0.02 | 0.19 | 0.11 |  |  |  |  |  |
| Queue Length 95th（m） | 0.9 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |  |  |
| Control Delay（s） | 9.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |  |  |
| Lane LOS | A | A |  |  |  |  |  |  |  |  |  |  |
| Approach Delay（s） | 9.1 | 0.0 | 0.0 |  |  | 0.0 |  |  |  |  |  |  |
| Approach LOS | A | A |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.2 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 24．5\％ |  | Level | rvice |  |  | A |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |





## 2024 Background Traffic Only

|  | * |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBT | SBL | SBR |
| Lane Configurations | ${ }^{*}$ | 44 | 中 ${ }^{\text {a }}$ | ${ }^{1}$ | F |
| Traffic Volume (vph) | 362 | 687 | 671 | 70 | 172 |
| Future Volume (vph) | 371 | 704 | 688 | 72 | 176 |
| Lane Group Flow (vph) | 393 | 747 | 796 | 76 | 187 |
| Turn Type | pm+pt | NA | NA | Prot | Perm |
| Protected Phases | 7 | 4 | 8 | 6 |  |
| Permitted Phases | 4 |  |  |  | 6 |
| Detector Phase | 7 | 4 | 8 | 6 | 6 |
| Switch Phase |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 9.5 | 22.5 | 22.5 | 22.5 | 22.5 |
| Total Split (s) | 15.0 | 37.5 | 22.5 | 22.5 | 22.5 |
| Total Split (\%) | 25.0\% | 62.5\% | 37.5\% | 37.5\% | 37.5\% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Lead/Lag | Lead |  | Lag |  |  |
| Lead-Lag Optimize? | Yes |  | Yes |  |  |
| Recall Mode | None | None | None | Max | Max |
| Act Effct Green (s) | 31.8 | 31.8 | 16.8 | 18.0 | 18.0 |
| Actuated g/C Ratio | 0.54 | 0.54 | 0.29 | 0.31 | 0.31 |
| v/c Ratio | 0.89 | 0.39 | 0.79 | 0.14 | 0.30 |
| Control Delay | 37.0 | 8.6 | 25.6 | 16.2 | 4.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 37.0 | 8.6 | 25.6 | 16.2 | 4.6 |
| LOS | D | A | C | B | A |
| Approach Delay |  | 18.4 | 25.6 | 8.0 |  |
| Approach LOS |  | B | C | A |  |
| Queue Length 50th (m) | 26.4 | 23.3 | 42.4 | 6.4 | 0.0 |
| Queue Length 95th (m) | \#73.5 | 33.6 | 61.3 | 14.9 | 12.1 |
| Internal Link Dist (m) |  | 153.3 | 86.2 | 122.6 |  |
| Turn Bay Length (m) |  |  |  |  | 80.0 |
| Base Capacity (vph) | 443 | 1987 | 1081 | 542 | 614 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.89 | 0.38 | 0.74 | 0.14 | 0.30 |
| Intersection Summary |  |  |  |  |  |
| Cycle Length: 60 |  |  |  |  |  |
| Actuated Cycle Length: 58.8 |  |  |  |  |  |
| Natural Cycle: 60 |  |  |  |  |  |
| Control Type: Actuated-Uncoordinated |  |  |  |  |  |
| Maximum v/c Ratio: 0.89 |  |  |  |  |  |
| Intersection Signal Delay: 19.8 |  |  |  |  | ersection |
| Intersection Capacity Utilization 56.0\% |  |  |  |  | Level of |
| Analysis Period (min) 15 |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |

Splits and Phases: 10: Wyse \& Thistle


|  | $\rangle$ |  | 7 | $\checkmark$ |  |  | 4 | $\dagger$ | $p$ |  | $\frac{1}{\dagger}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | 「 |  |  | 「 |  | 44 | 「 |  | 4t |  |
| Traffic Volume（veh／h） | 0 | 0 | 30 | 0 | 0 |  | 0 | 764 | 0 | 0 | 448 | 20 |
| Future Volume（Veh／h） | 0 | 0 | 31 | 0 | 0 | 0 | 0 | 783 | 0 | 0 | 459 | 21 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | －5\％ |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate（vph） | 0 | 0 | 33 | 0 | 0 | 0 | 0 | 830 | 0 | 0 | 487 | 22 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width（m） |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed（m／s） |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | None |  |  | None |  |
| Median storage veh） |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal（m） |  |  |  |  |  |  |  | 53 |  |  | 45 |  |
| pX，platoon unblocked | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.91 | 0.94 |  |  | 0.91 |  |  |
| vC ，conflicting volume | 913 | 1328 | 254 | 1106 | 1339 | 415 | 509 |  |  | 830 |  |  |
| vC 1 ，stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 508 | 948 | 85 | 713 | 960 | 170 | 355 |  |  | 624 |  |  |
| tC，single（s） | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 |  |  | 4.1 |  |  |
| $\mathrm{tC}, 2$ stage（s） |  |  |  |  |  |  |  |  |  |  |  |  |
| tF（s） | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \％ | 100 | 100 | 96 | 100 | 100 | 100 | 100 |  |  | 100 |  |  |
| cM capacity（veh／h） | 422 | 244 | 901 | 289 | 240 | 771 | 1130 |  |  | 870 |  |  |
| Direction，Lane \＃ | EB 1 | WB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 |  |  |  |  |  |
| Volume Total | 33 | 0 | 415 | 415 | 0 | 325 | 184 |  |  |  |  |  |
| Volume Left | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |  |  |
| Volume Right | 33 | 0 | 0 | 0 | 0 | 0 | 22 |  |  |  |  |  |
| CSH | 901 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |  |  |  |  |  |
| Volume to Capacity | 0.04 | 0.05 | 0.24 | 0.24 | 0.02 | 0.19 | 0.11 |  |  |  |  |  |
| Queue Length 95th（m） | 0.9 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |  |  |
| Control Delay（s） | 9.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |  |  |
| Lane LOS | A | A |  |  |  |  |  |  |  |  |  |  |
| Approach Delay（s） | 9.1 | 0.0 | 0.0 |  |  | 0.0 |  |  |  |  |  |  |
| Approach LOS | A | A |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.2 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 24．5\％ |  | Level | rvice |  |  | A |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |





## 2024 Background and Development

|  | 4 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBT | SBL | SBR |
| Lane Configurations | \% | 44 | 中t | ${ }^{*}$ | 7 |
| Traffic Volume (vph) | 362 | 687 | 671 | 70 | 172 |
| Future Volume (vph) | 371 | 704 | 694 | 79 | 182 |
| Lane Group Flow (vph) | 403 | 765 | 824 | 86 | 198 |
| Turn Type | pm+pt | NA | NA | Prot | Perm |
| Protected Phases | 7 | 4 | 8 | 6 |  |
| Permitted Phases | 4 |  |  |  | 6 |
| Detector Phase | 7 | 4 | 8 | 6 | 6 |
| Switch Phase |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 9.5 | 22.5 | 22.5 | 22.5 | 22.5 |
| Total Split (s) | 15.0 | 37.5 | 22.5 | 22.5 | 22.5 |
| Total Split (\%) | 25.0\% | 62.5\% | 37.5\% | 37.5\% | 37.5\% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Lead/Lag | Lead |  | Lag |  |  |
| Lead-Lag Optimize? | Yes |  | Yes |  |  |
| Recall Mode | None | None | None | Max | Max |
| Act Effct Green (s) | 32.1 | 32.1 | 17.0 | 18.0 | 18.0 |
| Actuated g/C Ratio | 0.54 | 0.54 | 0.29 | 0.30 | 0.30 |
| v/c Ratio | 0.92 | 0.40 | 0.81 | 0.16 | 0.32 |
| Control Delay | 41.6 | 8.6 | 26.7 | 16.5 | 4.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 41.6 | 8.6 | 26.7 | 16.5 | 4.6 |
| LOS | D | A | C | B | A |
| Approach Delay |  | 20.0 | 26.7 | 8.2 |  |
| Approach LOS |  | B | C | A |  |
| Queue Length 50th (m) | 28.2 | 24.0 | 44.4 | 7.2 | 0.0 |
| Queue Length 95th (m) | \#77.1 | 34.6 | \#65.1 | 16.4 | 12.4 |
| Internal Link Dist (m) |  | 153.3 | 86.2 | 122.6 |  |
| Turn Bay Length (m) |  |  |  |  | 80.0 |
| Base Capacity (vph) | 440 | 1978 | 1076 | 540 | 620 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.92 | 0.39 | 0.77 | 0.16 | 0.32 |
| Intersection Summary |  |  |  |  |  |
| Cycle Length: 60 |  |  |  |  |  |
| Actuated Cycle Length: 59.1 |  |  |  |  |  |
| Natural Cycle: 65 |  |  |  |  |  |
| Control Type: Actuated-Uncoordinated |  |  |  |  |  |
| Maximum v/c Ratio: 0.92 |  |  |  |  |  |
| Intersection Signal Delay: 20.9 |  |  |  |  | rsection |
| Intersection Capacity Utilization 56.0\% |  |  |  |  | Level of |
| Analysis Period (min) 15 |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |

Splits and Phases: 10: Wyse \& Thistle




## APPENDIX E

## Alternate Driveway Evaluation

fathomstudio.ca
1 Starr Lane
Dartmouth, NS
B2Y 4V7
$\qquad$

## Issued

March 23, 2020
Project Number
F: 19-041

Mr. Alex Dunphy
via: Email to dunphy.alex@gmail.com

## Wyse Road Development - Alternate Driveway Locations

Dear Mr. Dunphy,

This letter was prepared in response to the request to evaluate alternate access points to the Wyse Road Development and specifically the feasibility of access driveways off Wyse Road and / or Nantucket Avenue. The development is located in the northeast corner of the intersection of Wyse Road with Nantucket Avenue and the Macdonald Bridge approach with overall traffic operations being addressed in a Transportation Impact Study prepared by Fathom Studio in November 2019.

The original proposed location for the development driveway was off the west entrance roadway to the Dartmouth Sportsplex coinciding with one of the two existing driveways at the north end of the site's parking lot that serviced the previous development. Recent decisions have indicated that the original driveway location is no longer a feasible option therefore alternate access points to the site's underground parking structure off Nantucket Avenue or Wyse Road were explored as shown in the figure below.


The original transportation impact study estimated that between 70 and 80 trips enter and exit the building during the peak hours of traffic (just over one trip per minute) and that the added traffic volumes have very little impact to operations on the adjacent road network. Operationally, we do not expect the alternate driveway locations to change these conclusions. The impacts and implications of each access option is discussed in greater detail on the following pages.
fathomstudio.ca 1 Starr Lane Dartmouth, NS B2Y 4V7

## Driveway to Wyse Road

A driveway to Wyse Road would be located near the east end of the property approximately 40 meters east of the nearest Nantucket Avenue curb line and 45 meters west of the nearest curb line of the existing Wyse Road driveway to the Dartmouth Sportsplex.
At that location Wyse Road is 7-lanes wide consisting of:

- 2 eastbound through lanes;
- 1 eastbound added lane receiving traffic from the Macdonald Bridge right turn channelization;
- 2 westbound left turn lanes to the Macdonald Bridge;
- 1 westbound transit priority lane allowing buses to turn left onto the bridge; and,
- 1 westbound shared through / right turn lane with a channelized right turn to Nantucket Avenue.
The proposed driveway location is in relatively close proximity to the Nantucket/ Wyse Road intersection. Challenges created by the wide cross-section and diversity of lane uses suggest that this driveway be configured as a right-in, rightout (RIRO) access to the development's underground parkade. RIRO operations would require that all entering movements take place from the westbound curb lane of Wyse Road.

Vehicles approaching from east of the site (Downtown Dartmouth for example) will approach the driveway on Wyse Road with little inconvenience. Vehicles approaching from the south (Macdonald Bridge), west (Wyse Road, Victoria Road) and north (Thistle, Woodland Ave.) would be required to select routing that would allow them to access the westbound curb lane on Wyse Road. While this may increase travel distances slightly, there are numerous nearby options to gain access to the parkade entrance.

With respect to exiting movements, vehicles destined to the west and north would operate with little inconvenience. Vehicles destined to the south or east will be required to find routing options to support their trip which ultimately depends on their destination.

Other considerations that are relevant to a driveway on Wyse Road:

- The westbound through/right lane on Wyse Road has some of the lowest traffic volumes at the Wyse / Nantucket intersection and therefore entry and exit movements should be relatively easy to make;
- There is an existing driveway to the property at this location;
- Being close to the traffic signals at Wyse and Nantucket and on the upstream side, entry and exit movements will frequently (particularly during the AM peak hour) take place adjacent to vehicle queues in the double left turn lane and occasionally bus queues in the dedicated westbound bus lane;
- During off peak hours, it is expected that some vehicles may directly access the double left turn lanes onto the Bridge, and some could attempt to make a left turn exiting movement; and,
- Consideration should be given to appropriate signage and potentially a channelized island between the entry and exit lanes to deter left turn movements to and from the driveway.
fathomstudio.ca
1 Starr Lane
Dartmouth, NS
B2Y 4V7

The Nantucket Avenue driveway option would be located between Wyse Road and the existing western driveway to the Dartmouth Sportsplex. The distance between these two nearest curb lines is about 85 meters, which is similar to the Wyse Road spacing. It is anticipated that the driveway would be located approximately halfway between Wyse Road and the Sportsplex driveway, though exact positioning will need to be coordinated with the building design requirements.

Adjacent to this driveway, Nantucket Avenue is 5 lanes wide consisting of:

- 2 northbound through lanes with the median lane sharing a left turn movement into the Dartmouth Shopping Center and ESSO gas station;

- 1 right turn only lane that enters the Dartmouth Sportsplex driveway. North of the Sportsplex driveway, this lane transitions to a transit only lane that enters the Dartmouth Bridge Transit Terminal. Buses coming across the Macdonald Bridge have a signed dedicated lane to access this curb lane (though this lane is frequently used by regular vehicles) meaning drivers intending to turn right into the Sportsplex should make a lane change to the curb lane after clearing the Wyse Road intersection.
- 2 southbound through lanes to the Macdonald Bridge with the curb lane being shared as a channelized right turn movement to Wyse Road. Left turns are not permitted in the southbound direction.

Similar to the Wyse Road driveway alternative, lane configurations, vehicle movements and volumes suggest that the access be configured as a right-in, rightout (RIRO) driveway. One-way operations would require that all entering movements take place from the northbound curb lane of Nantucket Avenue.

Vehicles approaching from the south, east and west on Wyse Road can access the driveway with little inconvenience and vehicles approaching from the north would have to make minor route adjustments to Thistle Street or Boland Road to access northbound Nantucket to the entrance driveway. Exiting movements to the north are straightforward and movements to the east and west would have to use Victoria Road instead of Wyse Road but still remain relatively convenient. Movement to the Macdonald Bridge are more challenging requiring drivers to use alternate routing.

Other considerations that are relevant to an alternate driveway on Nantucket Road include:

- The northbound curb lane is already configured for right turns only;
- The driveway is close to the traffic signals at Wyse and Nantucket and on the downstream side meaning vehicles are still traveling relatively slowly, though cars will be part of a platoon once the northbound signals turn green at Wyse Road;
- There is unlikely to be significant congestion adjacent to the driveway as traffic is generally free flowing past the driveway. Queues from the pedestrian signals located immediately to the north generally occur in the two through lanes and right turning traffic is generally lower and not impeded by the signals;
fathomstudio.ca
1 Starr Lane
Dartmouth, NS
B2Y 4V7
- The driveway is adjacent to an area that is subject to some lane change activity (though limited weaving) and frequent bus traffic. The busiest periods adjacent to this driveway would be during the PM peak hour of traffic;
- During off peak hours, it is possible that some vehicles may attempt to make left turns to or from the driveway. These are considered undesirable and have safety implications therefore options such as extending the median on Nantucket Avenue past the driveway may be warranted; and,
- Consideration would have to be given to signage and potentially a channelized island between the entry and exit lanes to deter left turn movements to and from the driveway.


## Conclusions and Discussions

Two alternative access option were identified in this letter including one on Wyse Road and one on Nantucket Avenue. Both options are feasible from an external traffic perspective as well as from an internal building design perspective. As both intersections operate in relative close proximity to the signalized intersection at Nantucket, Wyse and the Macdonald Bridge, the detailed design process for this project will need to specifically address geometric, operational and safety elements of the driveway intersections (including pedestrian crossings) to provide a safe and controlled access to the site.

It is important to remember that volumes to and from driveways for this development are very low, which helps reduce the potential impacts of any risk factors that may be present. While there may be minor inconveniences to some drivers due to the right-in, right-out restrictions, there are a wide variety of route options adjacent to the site to minimize any such inconveniences.

The area is highly commuter oriented with direct access to robust transit service and active transportation networks. It is expected that this development will be viewed positively by a higher percentage of residents due to the existing alternative modal opportunities. Furthermore, there are significant initiatives underway in HRM to further promote transit ridership and active transportation modes of travel. This development is exceptionally well positioned to take advantage of these initiatives and these collective opportunities appear to significantly outweigh any minor inconveniences that drivers of private passenger vehicles may experience due to the left turn restrictions at the driveway.
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Should you have any questions regarding the content of this letter, or require any additional information, please contact the undersigned at (902) 233-1152, or by email at Roger.Boychuk@FathomStudio.ca.

Yours sincerely,

## Original Signed

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